

MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS-1963-A

CRC Report No. 538



TWO-TEMPERATURE VAPOR LOCK AND HIGH-TEMPERATURE DRIVEABILITY PERFORMANCE OF 1982 PASSENGER VEHICLES

December 1984



MIC FILE COPY

85

COORDINATING RESEARCH COUNCIL, INC. 219 PERIMETER CENTER PARKWAY, ATLANTA, GEORGIA 30346 The Coordinating Research Council, Inc. (CRC) is a nonprofit corporation supported by the petroleum and automotive equipment industries. CRC operates through committees made up of technical experts from industry and government who voluntarily participate. The four main areas of research within CRC are: air pollution (atmospheric and engineering studies); aviation fuels, lubricants, and equipment performance; heavy-duty vehicle fuels, lubricants, and equipment performance (e.g., diesel trucks); and light-duty vehicle fuels, lubricants, and equipment performance (e.g., passenger cars). CRC's function is to provide the mechanism for joint research conducted by the two industries that will help in determining the optimum combinations of petroleum products and automotive equipment. CRC's work is limited to research that is mutually beneficial to the two industries involved, and all information is available to the public.

COORDINATING RESEARCH COUNCIL

INCORPORATED

219 PERIMETER CENTER PARKWAY AYLANTA. GEORGIA 30346 (404) 396-3400

TWO-TEMPERATURE VAPOR LOCK AND HIGH-TEMPERATURE DRIVEABILITY PERFORMANCE OF 1982 PASSENGER VEHICLES (CRC Project No. CM-118-82)

IN FORMULATING AND APPROVING REPORTS, THE APPROPRIATE COMMITTEE OF THE COORDINATING RESEARCH COUNCIL, INC. HAS NOT INVESTIGATED OR CONSIDERED PATENTS WHICH. MAY APPLY TO THE SUBJECT MATTER. PROSPECTIVE USERS OF THE REPORT ARE RESPONSIBLE FOR PROTECTING THEMSELVES AGAINST LIABILITY FOR INFRINGEMENT OF PATENTS.

Prepared by the
1982 Analysis Panel
of the
CRC Volatility Group

December 1984

Light-Duty Vehicle Fuel, Lubricant, and Equipment Research Committee of the

Coordinating Research Council, Inc.

ABSTRACT

MZ,

The 1982 CRC High-Temperature Driveability Program was conducted at the US Army Proving Grounds near Yuma, Arizona, from September 20 through October 19, 1982, at nominal ambient temperatures of 70°F (21.1°C) and 95°F (35°C). CRC has conducted previous programs for the evaluation of vapor lock and hot start and driveability of 1971 and 1975 model passenger cars. Since 1975, vehicle designs have changed rapidly to meet more stringent exhaust emissions and fuel economy standards. These changes may affect vehicle high-temperature performance. The 1982 CRC High-Temperature Driveability Program investigated the effect of such changes on vapor lock performance of nineteen 1982 passenger vehicles at nominal temperatures of 70°F (21°C) and 95°F_(35°C)> The two_≂temperature vapor lock evaluation was used in updating ambient temperature corrections of volatility over a range of temperature from 70°F (21°C) to 95°F (35°C) Hot-start and drive-ability performance was evaluated at a nominal 95°F (35°C) temperature by two test procedures. A new city driveability procedure emphasized conditions that could cause performance problems encountered in heavy stop-and-go traffic after a period of temperature stabilization. Selected vehicles were also evaluated using the CRC Hot-Start and Driveability Procedure.

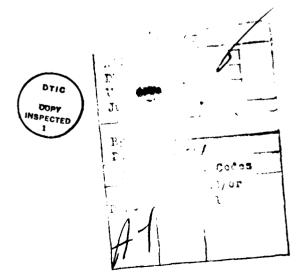


TABLE OF CONTENTS

TEXT		<u>Page</u>
	ABSTRACT	i
I.	INTRODUCTION	1
II.	SUMMARY	2
III.	TEST VEHICLES	3
IV.	TEST FUELS	3
٧.	TEST FACILITIES	4
VI.	TEST TECHNIQUES	6
	A. 1975 CRC Vapor Lock Technique B. Alternate Vapor Lock Procedure C. CRC Hot-Start and Driveaway Technique D. City Driveability Procedure	6 6
VII.	TEST DESIGN	8
VIII.	AMBIENT CONDITIONS	8
IX.	ON-SITE DATA RECORDING AND PROCESSING	8
Х.	DISCUSSION OF RESULTS	9
	A. Vapor Lock	11
TABLES		
Tab Tab Tab	The I - Description of Test Cars	18
Tab	le VII - Test Vehicle Vapor Lock and City Driveability	23

TABLES - (Continued)	o age
Table VIII - Carburetor Fuel Line Temperatures for	
95°F(35°C) Vapor Lock Tests	
70°F(21°C) Vapor Lock Tests	
Table XI - Fuel Pump Inlet and Fuel Tank Temperatures	
for 70°F(21°C) Vapor Lock Tests	
FIGURES	
Figure 1 - Temperature at V/L=20 and Percent Evaporated	20
at 158°F Versus Reid Vapor Pressure Figure 2 - Test Course	
Figure 3 - Distribution of Limiting Ty/L=20 for Three Model Years at 95°F(35°C)	21
Figure 4 - Distribution of Limiting T _{V/L=20} at 70°F (21°C) and 95°F(35°C)	
Figure 5 - Distribution of Limiting T _{V/L=20} of 1982 Model Year Cars Equipped with Fuel-Return	
Versus Non-Fuel-Return Lines	
Figure 7 - Vehicle Ranking: Vapor Lock Versus Hot Start and Driveaway (By Car Number)	35
APPENDICES	
APPENDIX A - Program Participants and Panel MembershipsA	-1
APPENDIX B - Program: 1982 CRC High-Temperature Driveability ProgramB	i-1
APPENDIX C - Fuel Inspection Data	-1
APPENDIX D - Test Procedures and Data Rating Systems) - 1
APPENDIX E - Rater Comparisons - City Driveability ProcedureE	-1
APPENDIX F - Effects of Fuel Volatility Changes - City Driveability ProcedureF	-1
ADDENDITY C 1002 CDC Vanon Lock Took Date	

I. INTRODUCTION

The 1982 CRC High-Temperature Driveability Program was conducted at the US Army Proving Grounds near Yuma, Arizona, from September 20 through October 19, 1982. The series of road tests comprising the program were conducted at nominal ambient temperatures of 70°F (21°C) and 95°F (35°C).

CRC has conducted previous programs for the evaluation of vapor lock and hot start and driveaway of 1971 and 1975 model passenger cars. Since 1975, vehicle designs have changed rapidly to meet more stringent exhaust emissions and fuel economy standards. These changes may affect vehicle high-temperature performance. The 1982 CRC High-Temperature Driveability Program investigated the effect of such changes on vapor lock performance of nineteen 1982 passenger vehicles at nominal temperatures of 70°F (21°C) and 95°F (35°C). The vapor lock tolerance of each vehicle was determined for each temperature by evaluating incremental blends from a fuel series ranging in volatility from approximately 7.0 to 17.0 psi Reid vapor pressure. Various blends were tested to determine the fuel which would give a 25 percent increase in acceleration time relative to a base acceleration. This fuel in terms of $T_{\gamma/L=20}$ defined the vapor lock tolerance of the vehicle. The two-temperature vapor lock evaluation was used in updating ambient temperature corrections of volatility over a range of temperature from 70°F (21°C) to 95°F (35°C). In addition, an alternate vapor lock procedure was run in two vehicles.

Hot-start and driveaway performance was evaluated at a nominal 95°F (35°C) temperature by two test procedures. A new test procedure that emphasized low speed, mild acceleration, and frequent idle periods was evaluated in this program. This City Driveability Procedure emphasized conditions that could cause performance problems encountered in heavy stop-and-go traffic after a period of temperature stabilization. A special pentane-rich fuel and one or more vapor lock fuels were tested in all vehicles using the City Driveability Procedure. Eleven of the vehicles were also evaluated using the CRC Hot-Start and Driveaway Procedure. Performance was expressed for both procedures in terms of CRC demerits, with poorer performance resulting in higher demerit levels.

Appendix A lists participants in the test program, members of the Program Panel, and members of the Data Analysis and Report-Writing Panel. The program proposal approved by the CRC Volatility Group is shown in Appendix B.

II. SUMMARY

- Vapor lock severity increased in most cases as fuel volatility and ambient temperature increased.
- The 1982 model cars tested had fewer vapor lock problems than 1975 and 1971 model cars tested in previous CRC programs. A fuel with T_{V/L=20} of 124°F (ASTM Class C) satisfied 75 percent of 1982 model cars, 45 percent of 1975 model cars, and 20 percent of 1971 model cars at 95°F.
- For vapor lock tests, the ambient temperature correction factor for adjusting $T_{V/L=20}$ data was established to be 0.7°F $T_{V/L=20}$ per degree ambient temperature.
- There appeared to be no appreciable difference in vapor lock performance for cars with and without fuel return lines.
- The limiting vapor lock requirements were outside the range of test fuels for five of nineteen cars at a nominal 95°F (35°C) test temperature, and for seven of nineteen cars at a nominal 70°F (21°C) test temperature.
- Ten of twelve cars at their critical soak condition had more severe vapor lock requirements at 95°F (35°C) than at 70°F (21°C).
- Twelve of fourteen cars were idle soak limited at 95°F (35°C). At 70°F (21°C), six of twelve cars were idle soak limited, and six were key-off soak limited.
- Data did not establish a definitive relationship between a vehicle's vapor lock tolerance and its hot-start and driveaway performance.
- For the City Driveability Procedure, seven vehicles showed large changes in demerit levels with changes in fuel volatility.
- Both the City Driveability Procedure and the CRC Hot-Start and Driveaway Procedure showed volatility and vehicle effects.
- From these data, there is no clear advantage to recommend either the City Driveability Procedure or the CRC Hot-Start and Driveaway Procedure for driveability evaluations.

III. TEST VEHICLES

Eighteen passenger cars and one passenger van were tested in this program. Selection was based upon a list of twenty primary and five secondary vehicles listed in the test plan, contingent upon availability from rental agencies. In the selection of test cars, consideration was given to sales volume and vehicles of special interest. All vehicles were equipped with automatic transmissions, air conditioning, and Federal exhaust emission control devices. Vehicles are described in detail in Table I.

Prior to the start of the test program, the vehicles were delivered to a contractor for test preparation. Car preparation included installation of fuel tank drains, installation of a vacuum tee, checking and adjusting timing and idle speed, and checking integrity of emission control equipment. Thermocouples were installed on test vehicles by test participants at the start of the test program. One thermocouple was taped to the exterior of the fuel line as close to the carburetor or fuel injector as possible. For General Motors vehicles, a second thermocouple was installed in the fuel tank through the drain line. For all other vehicles, a second thermocouple was taped to the exterior of the fuel line as close to the fuel pump inlet as possible. At the conclusion of the test, the vehicles were returned to the contractor for removal of the tank drains. A flat 3/32-inch brass plate was soldered over the tank drain hole.

IV. TEST FUELS

Vapor lock test fuels consisted of three base fuels of 7.1, 11.8, and 16.3 psi Reid vapor pressure (RVP) identified as RMFV 90-82, 91-82, and 92-82, respectively. The fuel series design accommodated a 10.5 psi RVP fuel as representative of a typical summer fuel, and a 13.5 psi RVP fuel as representative of a typical winter fuel. Increased volatility was accomplished primarily by the addition of butane. Intermediate test fuels were blended on-site using two blending pumps. One blending pump dispensed the low and intermediate volatility fuels and blends of the low and intermediate fuels. The other pump dispensed the intermediate and high volatility fuels and blends of the intermediate and high fuels. Table II presents the average fuel inspection data for the odd number fuels available from the blend pumps. The blends were prepared by one laboratory and were shipped to participating laboratories for analysis. Individual inspection data by participating laboratories are presented in Appendix C.

Figure 1 shows the relationship of $T_{V/L=20}$ and percent evaporated at 158°F to RVP for the series of vapor lock fuels. The curves in Figure 1 correspond to least-squares equations; the fuel series curves were used to derive the other volatility values from measured RVP's when processing data from the vapor lock and driveability tests:

$$T_{V/L=20} \approx 213.05 - 9.9293 (RVP) + 0.19306 (RVP2)$$

%@158°F = 5.94 + 1.8945 (RVP) - 0.0099081 (RVP²)

A special fuel blend (RMFV 93-82), shown in Table II as Fuel 20 and used in simulated low-speed city driving tests, was intended to emphasize problems in the hot-start and driveaway application. It was a pentane-rich high volatility fuel. In order to relate other properties to measured RVP's on tank samples subjected to weathering during the road tests, samples of this fuel were allowed to evaporate to varying degrees, then RVP and T versus V/L curves were determined onsite at Yuma on the fresh and weathered samples. Subsequently, a retain sample was also weathered in several stages, and RVP and ASTM D 86 distillations were determined on the fresh and weathered portions at one of the cooperating laboratories. Data points and least-square curves for $T_{V/L=20}$ and percent evaporated at 158°F versus RVP of weathered RMFV 93-82 fuel are shown in Figure 1, along with corresponding curves for the vapor lock fuels. Equations for the volatility relations of weathered Fuel 20 are:

$$T_{V/L=20} = 215.71 - 9.919 (RVP) + 0.1758 (RVP2)$$

%@158°F = -10.524 + 3.9496 (RVP)

(For percent evaporated at 158°F, the linear equation fit the data as well as a second-order equation and was, therefore, used. Since the data were obtained in only one cooperating laboratory, the constant term in the equation was adjusted to match the point for the all-laboratory average RVP and percent evaporated at 158°F.)

V. TEST FACILITIES

Facilities made available for the test work at the US Army Yuma Proving Ground included a five-mile test track, fuel storage, a soak shelter, a cold room for fuel dispensing, and a petroleum testing laboratory. A fork-lift truck, a refrigerated trailer, a temporary soak shelter to accommodate three vehicles, and a mobile office trailer were provided by CRC.

The test course, shown in Figure 2, consisted of the following:

- Yuma Proving Ground Dynamometer Course level blacktop with two-mile straightaway and half-mile loops at each end
- Gravel roads, one to two miles long, running between the dynamometer course and Arizona Highway Route 95
- A 7.5-mile section of essentially level blacktop highway -Arizona Highway Route 95

Car warm-up was achieved by proceeding from the dynamometer course via a gravel road to the highway, driving fifteen miles on the highway, returning to the dynamometer course to complete one lap around the course (five miles), and then proceeding to the soak shelter. All vapor lock and hot-start and driveaway evaluations were conducted on the dynamometer course.

Three roofless soak shelters, twelve feet by twenty-four feet and constructed of plywood with plastic end curtains, were used primarily for vapor lock testing. A permanent twenty-foot by forty-foot roofless soak shelter with doors at both ends was used primarily for hotstart and driveaway tests.

Dry-bulb air temperature was recorded at the soak area of the dynamometer test track at fifteen-minute intervals while testing was in progress.

On-site fuel analyses were performed in the Yuma Proving Ground Petroleum Laboratory. Reid vapor pressure was determined using an automatic RVP instrument supplied by Southwest Research Institute.

A refrigerated trailer van was used for the bulk storage of all test fuels, except the low volatility vapor lock fuel, which was stored outdoors. Daily fuel supplies were stored in a large walk-in refrigerator, and were dispensed to the test cars through two blend pumps. Fuel 20 was distributed through a separate portable pump. Both the refrigerator and refrigerated trailer were maintained at approximately 40°F.

Duplicate samples were taken from the fuel tanks, through the drain line, in one-quart bottles using a Quick-Chill Sampling Apparatus. Samples were taken through the drain line to prevent significant loss of tank pressure during sampling. For all tests, samples were taken during the soak and idle periods.

VI. TEST TECHNIQUES

The 1982 CRC High-Temperature Driveability Program used four test techniques, two for vapor lock and two for hot start and driveaway:

- 1975 CRC Vapor Lock Technique
- An alternate vapor lock technique which alters the timing of the accelerations
- CRC Hot-Start and Driveaway Technique
- City Driveability Procedure

A. 1975 CRC Vapor Lock Technique

The primary vapor lock technique used in this program was the same as used in the 1975 CRC High-Temperature Driveability Program. Vapor lock was evaluated at both 70°F (21°C) and 95°F (35°C). This technique and the data rating system used are described in detail in Appendix D. In brief, the percent gain in acceleration time may be established on any one fuel by comparing a wide-open-throttle acceleration, following a prescribed idle or soak period, with the average for base accelerations obtained during the warm-up operation. The limiting volatility for a 25 percent increase in acceleration time may then be defined by bracketing with fuels which produced higher or lower acceleration times.

B. Alternate Vapor Lock Procedure

A few runs were made with an alternate vapor lock technique that altered the timing of the accelerations. The procedure used was the same as the 1975 CRC Vapor Lock Technique, with the exception that the timed acceleration was from 0 to 30, 50, and 60 mph, instead of from 15 to 50, 60, and 70 mph.

C. CRC Hot-Start and Driveaway Technique

The CRC Hot-Start and Driveaway Procedure is described in detail in Appendix D. Briefly, it consists of the following:

a. A prescribed warm-up during which a base start and run time are obtained.

- b. A ten-minute idle, followed by a back-up and abrupt stop at prescribed acceleration and deceleration rates.
- c. A series of accelerations of prescribed duration and rates, followed by prescribed decelerations and short idle periods.
- d. A twenty-minute engine-off soak, followed by a hot start and run of sixty seconds before driveaway.
- e. A repeat of Item c.

D. City Driveability Procedure

The City Driveability Procedure is a new hot-start and driveaway technique designed to appraise low-speed driveability and hot-starting problems. This new procedure was the primary driveability procedure used in the 1982 CRC High-Temperature Driveability Program, and was compared with the CRC Hot-Start and Driveaway Procedure for selected cars. The Procedure is described in detail in Appendix D. Briefly, it consists of the following:

- a. A prescribed warm-up.
- b. Simulated low-speed city traffic for four miles.
- c. A ten-minute idle soak, followed by an acceleration.
- d. Simulated low-speed city traffic for four miles.
- e. A twenty-minute key-off soak, followed by a hot start, followed by an acceleration.

For both driveability procedures, hesitation, stumble, surge, backfire, and stalls are recorded during acceleration and deceleration. Idle quality and stalls are recorded during idle periods, and cranking start time and total start time are recorded after engine-off soak. In addition to the number of times a malfunction occurs, the quality of all malfunctions, except stalls and start time, are evaluated as trace, moderate, or heavy. Sample data sheets are presented in Appendix D.

VII. TEST DESIGN

Since evaluation of vapor lock tolerance of the vehicle was necessary prior to hot driveability evaluations, only vapor lock testing for 95°F (35°C) was conducted for the first two days of the program, using four test crews. On the third day, the test crews were reassigned into five test crews: three vapor lock crews and two hot driveability crews. It was necessary to extend the test program a few days longer than had been originally planned in order to obtain the desired number of hot driveability test evaluations. By the end of the program, 115 95°F (35°C) vapor lock tests, 94 70°F (21°C) vapor lock tests, 66 City Driveability Procedure tests, and 20 CRC Hot-Start and Driveaway tests had been conducted. It was discovered during the test program that the low to intermediate blending pump had malfunctioned on October 4-6, dispensing 100 percent intermediate fuel for all settings. Although tests conducted during this time resulted in valid data, the desired volatility effects were not obtained for some runs.

VIII. AMBIENT CONDITIONS

Ambient conditions were not altogether favorable during the test program. During the first week, attempts were made to evaluate vapor lock at 70° F (21° C), but ambient temperatures were such that the maximum temperature was exceeded before completion of a test. During the second test week, temperatures did not exceed 90° F (32° C); therefore, no hot driveability or 95° F (35° C) vapor lock tests were conducted. During the third test week, high winds and cool temperatures precluded extensive testing. Although more normal conditions prevailed during the fourth week, temperatures were somewhat cooler than desired. To facilitate obtaining additional test hours, it was decided during the fourth week to reduce the starting temperature for hot driveability tests to 85° F (29° C) from 90° F (32° C).

IX. ON-SITE DATA RECORDING AND PROCESSING

Preliminary data processing was conducted on-site with the aid of a microcomputer and printer. Data recorded by the test crews were transcribed from the original data sheets (sample in Appendix D) to computerized spread sheets with similar data arrangement.

For vapor lock tests, average RVP's for duplicate samples were entered on each spread sheet. The computer program automatically calculated percent increases in acceleration time and fuel $T_{V/L=20}$, both unadjusted and adjusted to 70°F or 95°F (21°C or 35°C). Correlation used on-site to estimate $T_{V/L=20}$ from RVP were based on the supplier's fuel data. When volatility data were subsequently obtained on the vapor lock fuels from cooperative laboratories, the spread sheets were recalculated with new constants from the final correlation formula. Final printouts from the vapor lock tests are shown in Appendix G.

For driveability tests, the computer program calculated driveability demerits. Results from each driveability test occupy one entire page; therefore, only summary results are included in Appendix F. A complete set of driveability printouts is available for inspection at the CRC offices.

X. DISCUSSION OF RESULTS

A. Vapor Lock

Limiting T_{V/L=20}

Vapor lock limiting $T_{V/L=20}$ is shown in Table III for each car corrected to ambient temperatures of 95°F (35°C) and 70°F (21°C). This is the $T_{V/L=20}$ for a 25 percent increase in acceleration time at the most critical soak and speed condition. At 95°F (35°C), six of the nineteen cars tested were not fully characterized as to limiting volatility with the fuel series. Cars 2, 3, 8, 13, and 18 did not encounter vapor lock on the most volatile fuel tested. Car 1 encountered vapor lock with the least volatile fuel tested. Of the cars characterized for critical soak condition at 95°F (35°C), twelve were idle soak-limited, and two were engine-off soak-limited.

At 70°F (21°C), seven of the nineteen cars tested did not encounter vapor lock on the most volatile fuel tested, and were not, therefore, fully characterized as to limiting volatility. Of the cars characterized for critical soak condition at 70°F (21°C), six were idle soak-limited, and six were engine-off soak-limited. Of the twelve cars characterized for critical soak conditions at both temperatures, five cars which were idle limited at 95°F (35°C) were engine-off limited at 70°F (21°C), one car which was engine-off limited at 95°F (35°C) was idle limited at 70°F (21°C), and six cars had the same limiting condition at both temperatures.

Of the twelve cars for which limiting $T_{V/L=20}$ was obtained at 70°F (21°C), ten had higher $T_{V/L=20}$ for limiting vapor lock at 95°F (35°C). Two cars, 9 and 11, had higher $T_{V/L=20}$ for limiting vapor lock at 70°F (21°C). For these two cars, no explanation of the reversal of expected results was obtained.

2. Ambient Temperature Vapor Lock Corrections

Vapor lock tests were conducted over a range of $87^{\circ}F$ (30°C) to $111^{\circ}F$ (44°C) for $95^{\circ}F$ (35°C) vapor lock, and a range of $65^{\circ}F$ (18°C) to $85^{\circ}F$ (29°C) for $70^{\circ}F$ (21°C) vapor lock. The $T_{V/L=20}$ test data were corrected from actual ambient test conditions to nominal $95^{\circ}F$ (35°C) and $70^{\circ}F$ (21°C) temperatures using a previously established CRC expression, where:

Adjusted
$$T_{V/L=20}$$
 = Actual $T_{V/L=20}$ + K (or - Air Temperature) (70)
The K value used was K=1.

The 70°F (21°C) vapor lock tests were performed at both idle and engine-off soak conditions, so that comparable soak condition data would be available for both test temperatures. Comparable soak condition limiting $T_{V/L=20's}$ are shown in Table IV for the ten cars that were characterized at both test temperatures. The ten cars show an average limiting $T_{V/L=20}$ difference of 17.1 between the two test temperatures, giving a 0.68 $T_{V/L=20}$ correction for a one-degree change in ambient temperature. For convenience, the correction was rounded off to 0.7. The 0.7 factor is significantly different from the 1.0 previously used adjustment factor. It also shows a significant difference from a zero correction factor. With the exception of Table IV, all adjusted vapor lock data presented in this report use a K factor of 0.7 for ambient temperature correction.

3. Vapor Lock Distributions

Figure 3 shows distribution lines for limiting $T_{\gamma/L=20}$ for 95°F (35°C) for 1971 and 1975⁽¹⁾ cars tested in previous CRC programs compared with 1982 cars tested in this program. These data show a trend of decreasing vapor lock severity with more recent model year cars. A fuel with a 124°F (51°C) $T_{\gamma/L=20}$ would satisfy 20 percent of the 1971 cars tested, 45 percent of the 1975 cars tested, and 75 percent of the 1982 cars tested under the conditions of the CRC Vapor Lock Test at 95°F (35°C).

⁽¹⁾ Coordinating Research Council, Inc., "Driveability Performance of 1975 Passenger Cars at High Ambient Temperatures," CRC Report No. 490, November 1976.

The distribution of limiting $T_{V/L=20}$ values for the 1982 cars tested at 95°F (35°C) and 70°F (21°C) is shown in Figure 4 for their most severe soak and speed conditions. Six cars at 95°F (35°C) and seven cars at 70°F (21°C) had indeterminate values, because their requirements were outside the volatility range of the test fuels. The level of volatility distribution is different with the cars having a higher vapor lock severity at 95°F (35°C). The slopes of the distribution lines are different with a trend towards converging at the more severe vapor lock level.

The distribution of limiting $T_{V/L=20}$ values at 95°F (35°C) for 1982 cars with and without fuel return lines are shown in Figure 5. The slopes of the distribution lines are different, with the cars having fuel return lines showing a lower slope. There is no appreciable difference in vapor lock performance for cars with and without fuel return lines.

4. Alternate Vapor Lock Procedure

An alternate vapor lock procedure was run on two cars at 95°F (35°C). The alternate vapor lock procedure was the same as the CRC procedure, except accelerations were timed from 0 to 30, 50, and 60 mph. Limiting $T_{V/L=20's}$ for the alternate procedure and the CRC procedure are shown in Table V. Car 5 showed similar limiting $T_{V/L=20's}$ for both procedures. Car 14 was more severe on the CRC procedure. Based upon the limited data available, no conclusion can be reached as to the performance of this alternate procedure.

B. Comparison of City Driveability Procedure Versus CRC Hot-Start and Driveaway Procedure

In previous CRC tests, the CRC Hot-Start and Driveaway Procedure has shown it is capable of defining car performance in terms of fuel volatility. In this program, a limited number of tests were run using the CRC Hot-Start and Driveaway Procedure and a greater number were run using a new City Driveability Procedure. The purpose of these tests was to compare results of the two procedures and their ability to define car performance by segregating fuel effects. Detailed descriptions of both procedures are provided in Appendix D. The City Driveability Procedure includes thirty-four 0-20 mph accelerations, followed by idle periods and two 0-30 mph part-throttle accelerations. The CRC Hot-Start and Driveaway Procedure includes a back-up maneuver with moderate to severe braking, idle periods, and sixteen accelerations to different speeds at varied rates. Both procedures were completed by trained raters. Comparisons of trained rater results are provided in Appendix E.

In both cycles, driveability problems are quantified by assigning them numerical values that increase as problem severity increases. These values are termed "demerits;" large total demerit values are indicative of poor driveability. Seventeen comparison tests were completed in which the cars were run through both procedures with the same fuel and driver. The demerit values obtained are shown in Table VI. Average demerits of the City Driveability Procedure were about twice the average of the CRC Hot-Start and Driveaway Technique. The total weighted demerit (TWD) values for comparable runs are plotted in Figure 6. The linear relationship between the two cycles was:

TWD(CITY) = 1.48 TWD(CRC) + 92.6

$$R^2 = 0.23$$

Three cars were significantly more severe on the CRC procedure than the new procedure (cars 7, 9, and 14). Although no single driving problem caused the differences in demerits between the two procedures, demerits from driving stalls were about 34 to 51 percent higher for the CRC technique with the most volatile fuel. Correlation between the procedures was improved significantly when these cars were deleted from the model:

TWD(CITY) = 3.15 TWD(CRC) - 98.9

$$R^2 = 0.69$$

To segregate fuel effects, regression models typically are developed which relate fuel volatility characteristics (i.e., $T_{V/l=20}$, RVP, %0158°F, or distillation temperatures) to car per-Unfortunately, this fuel set was not designed to segregate volatility effects on driveability, nor were the tests performed in a balanced scheme which lends to proper model development. Consequently, models that identify the significant volatility parameter could not be developed for either test. Some regression work was completed with data from the City Driveability Procedure, but it is in a very general form (see Appendix F). Although the data indicate that both tests can separate fuels of different volatility, the ability of the new City Driveability Procedure versus the CRC Hot-Start and Driveaway Procedure to identify significant fuel parameters that affect car performance cannot be determined from this program. To evaluate the two test techniques, another program specifically designed to assess hot-weather driveability is required.

C. Comparison of Vapor Lock Versus City Driveability

To determine if there was a relationship between vapor lock performance and the City Driveability Procedure performance, a ranking was made of vapor lock and driveability performance. The ranking of the City Driveability Procedure performance was made with data obtained from the runs using the pentane-rich fuel (Fuel 20), since all nineteen cars were run on this fuel. The vehicles were ranked in order of decreasing vapor lock volatility tolerance and of increasing hot-start and driveaway total weighted demerits. These rankings are shown in Table VII and plotted in Figure 7. Those cars with undetermined limiting $T_{V/L=20}$ were ranked equally, and were not included in the data regression analysis. The regression line shown in Figure 7 has a positive slope of 0.34 and a coefficient of determination of 0.20. These data do not establish a strong relationship between a vehicle's vapor lock volatility tolerance and its city cycle hot-start and driveaway performance.

D. Fuel System Temperature Measurements

Fuel system temperatures were obtained on seventeen of the test vehicles for $95^{\circ}F$ ($35^{\circ}C$) vapor lock tests and for fourteen of the vehicles for $70^{\circ}F$ ($21^{\circ}C$) vapor lock tests. The following temperature measurements were obtained:

- o Surface temperature of the fuel line at the inlet to the carburetor or fuel injector for all vehicles.
- o Temperature of the fuel in the fuel tank for all General Motors vehicles.
- o Surface temperature of the fuel line at the inlet to the fuel pump for all non General Motors vehicles.

The average temperature of the fuel line at the inlet to the carburetor or fuel injector for all runs for each soak for each vehicle are listed in Tables VIII and IX for the 95°F (35°C) and 70°F (21°C) vapor lock tests, respectively. Tables X and XI show similar data for the fuel pump and fuel tank temperatures. Temperature data between idle and key-off soaks in some cases are not comparable. This is due to the nature of the vapor lock test, since after a few runs, idle or key-off is established as the limiting condition and further runs are not made on the non-limiting condition. In these cases, the number in parentheses is the average temperature for the runs in which both soak conditions were run.

There was no apparent correlation between vapor lock performance and fuel system temperatures. It would be expected that the critical soak condition that produced the highest carburetor and/or fuel pump temperature would be the most critical vapor lock condition. Table XII shows that for twelve cases, the most critical vapor lock soak condition also showed the highest carburetor and fuel pump temperatures. It also shows that for thirteen cases, the highest carburetor and/or fuel pump temperatures did not occur for the most critical vapor lock condition.

TABLES

AND

FIGURES

TABLE I

DESCRIPTION OF TEST CARS

(1982 Model Year)

Make	Model	Engine Disp., &	8	2	Fuel Return	Vehicle Identification No.	Fuel Inj.	Elec. F.P.	Emission System*
ujck ujck	Century Limited	3.0	> >	> >	ZZ	1G4AL19E4C0402668 1G4AM47A1CR110954	zz	ZZ	ಕಕ
adillac	Sedan DeVille	4.1	>	>	>-	1G6AV6982C9229870	>	>-	CL
hevrolet hevrolet	Cavalier	1.8	> >	>- 2	22	1G1AD69G7CC125391 1G1AB6RC9CA113775	2 2	ZZ	ರರ
hevrolet hevrolet	Citation Monte Carlo	3.2.8	- >- >-	: > >	: > Z	1G1AX68R8C6105093 1G1AZ37K50R157602	: > Z	: > Z	ಕರಕ
atsun	210	1.5	Z	>	>-	JN1PB025XCU692212	Z	z	10
ord	Club Wagon	9.4	>- >	>>	z >	1FMEE11E4CHA53342	ZZ	Z	ಕ
ora ord	Escort Granada	3.3°	- >-	 >-	- >-	1FABP27B0CA126399	zz	zz	ಕಕ
ord	Granada Mustang	3.8	>- >-	> >	>- >-	1FABP27B0CG127235 1FABP10A0CF147848	ZZ	zz	ಕಕ
incoln	Town Car	5.0	>	>	>-	1LNBP94FXCY621223	z	z	כר
onda	Accord	1.8	>	>	z	JHMSZ3427CC023143	z	>	10
ldsmobile	Cutlass	4.3	>	>	z	1G3AM6980CM480736	z	z	CL
lymouth	Reliant	2.2	>	>	>	1P3BP46B9CF223384	Z	z	บ
oyota	Corolla	1.8	>	>	Z	JT2TEL2L4C0738623	Z	z	OF
olkswagen	Rabbit	1.7	>-	>	>	1VWBB0174V010629	>	>	น

* CL = Closed Loop OL = Open Loop

IABLE 11
AVERAGE TEST FUEL PROPERTIES

Fuel No. RMFV	1 90-82	m ı	vn i		9 91-82	ε.	13	15	17 92-82	20 93-42
RVP, psi	7.1	8.2	9.3	9.01	11.8	13.1	14.2	15.4	16.3	13.4
1 _{V/L=20} , °f(°C)		152.5(66.9) 145.0(62.8) 137.2(58.4) 129.0(53.9) 123.0(50.5) 116.5(46.9) 110.3(43.5) 106.3(41.3)	137.2(58.4)	129.0(53.9)	123.0(50.5)	116.5(46.9)	110.3(43.5)	106.3(41.3)	102.2(39.0)	107.2(41.8)
Distillation (D-86) 1°F (1°C) @ X Evap.	6) 9.									
10	136 (57.8)	136 (57.8) 132 (55.5) 123 (50.5) 120 (48.9) 114 (45.5) 106 (41.1) 100 (37.8) 94 (34.4) 93 (33.9)	123 (50.5)	120 (48.9)	114 (45.5)	106 (41.1)	100 (37.8)	94 (34.4)	93 (33.9)	98 (36.7)
95	228 (108.9)	228 (108.9) 229 (109.4) 225 (107.2) 224 (106.7) 222 (105.5) 220 (104.4) 216 (102.2) 213 (100.5) 212 (100.0) 184 (84.4)	225 (107.2)	224 (106.7)	222 (105.5)	220 (104.4)	216 (102.2)	213 (100.5)	212 (100.0)	184 (84.4)
8	347 (175.0)	347 (175.0) 348 (175.5) 345 (173.9) 346 (174.4) 344 (173.3) 343 (172.8) 344 (173.3) 346 (174.4) 343 (172.8) 300 (148.9)	345 (173.9)	346 (174.4)	344 (173.3)	343 (172.8)	344 (173.3)	346 (174.4)	343 (172.8)	300 (148.9)
EP	417 (213.9)	417 (213.9) 418 (214.4) 416 (213.3) 417 (213.9) 416 (213.3) 416 (213.3) 414 (212.2) 414 (212.2) 414 (212.2) 415 (212.8)	416 (213.3)	417 (213.9)	416 (213.3)	416 (213.3)	414 (212.2)	414 (212.2)	414 (212.2)	415 (212.8)
API Gravity	56.8	97.6	58.5	59.4	60.4	61.4	62.1	63.0	63.8	74.4

TABLE III

LIMITING VAPOR LOCK AT 95°F(35°C) AND 70°F(21°C)

	9	5°F (35°C))	7	0°F (21°C)
Car	Critical Te	est Conditi	ion LT _{V/L=20}	Critical Te	st Condit	ion LT _{V/L=20}
No.	Hot Soak	Speed	°F (°C)	Hot Soak	Speed	°F (°C)
1	I	70	>150(>65.5)	ко	70	123 (50.5)
2			<108(<42.2)			<100(<37.8)
3			<103(<39.4)			< 97(<36.1)
4	KO	50,60,70	113 (45.0)	I	70	99 (37.2)
5	I	50	126 (52.2)	I	60	102 (38.9)
6	I	60,70	107 (41.7)	КО	50	105 (40.5)
7	I	50,60,70	113 (45.0)	ко	50,60,70	104 (40.0)
8			<113(<45.0)	***		< 99(<37.2)
9	I	60	119 (48.3)	ко	50	126 (52.2)
10	I	50,60,70	124 (51.1)	KO	50	118 (47.8)
11	KO	60,70	122 (50.0)	KO	70	130 (54.4)
12	I	60,70	125 (51.7)	I	70	103 (39.4)
13			<108(<42.2)			<106(<41.1)
14	I	60,70	124 (51.1)	I	70	103 (39.4)
15	I	70	121 (49.4)			<104(<40.0)
16	I	70	127 (52.8)	I	60,70	104 (40.0)
17	I	60,70	111 (43.9)			< 99(<37.2)
18			<111(<43.9)			<105(<40.5)
19	I	50	127 (52.8)	I	50	100 (37.8)

Note: I = Idle; KO = Key Off

TABLE IV

COMPARISON OF LIMITING TV/L=20 AT 95°F (35°C) AND 70°F (21°C)

Car	Soak <u>Condition</u>	Limiting T _{V/1} _95 (35)	L=20, °F (°C) _70 (21)	$\frac{\Delta}{\text{Limiting Ty/L=20}} (95-70)$
4	K0	114 (45.5)	99 (37.2)	15 (8.3)
5	I	126 (52.2)	98 (36.7)	28 (15.5)
7	I	110 (43.3)	100 (37.8)	10 (5.5)
9	I	118 (47.8)	116 (46.7)	2 (1.1)
10	I	123 (50.5)	107 (41.7)	16 (8.8)
11	KO	125 (51.7)	126 (52.2)	-1 (-0.5)
12	I	124 (51.1)	101 (38.3)	23 (12.8)
14	I	119 (48.3)	101 (38.3)	18 (10.0)
16	I	124 (51.1)	102 (38.9)	22 (12.2)
19	I	134 (56.7)	96 (35.5)	38 (21.2)

AVERAGE 17.1 (9.49)

CHANGE IN $T_{VL=20}$ /CHANGE IN AMBIENT TEMPERATURE 0.68°F (0.38°C)

Note: I = Idle; KO = Key Off

TABLE V

ALTERNATE VAPOR LOCK PROCEDURE VERSUS CRC VAPOR LOCK PROCEDURE

		CRC	A	LTERNATE
Car <u>No.</u>	Limiting Condition	LTV/L=20, °F(°C)	Limiting Condition	LTV/L=20; °F(°C)
5	Idle 15-50	125 (52.2)	Idle 0-30	127 (52.8)
14	Idle 15-60	124 (51.1)	Idle 0-60	116 (46.7)

TABLE VI

COMPARABLE DRIVEABILITY RUNS

			CRC				CITY	
Car	<u>Fuel</u>	TWD	empe)	rature °C	T	WD	lempe: °F	rature °C
1	1	263	89.3	31.8	-	57	82.0	27.8
2	20	130	88.8	31.5		99	92.6	33.7
2	17	124	92.3	33.5		26	87.6	30.9
3	20	47	93.0	33.9		64	99.4	37.4
3	17	 97	91.0	32.8		86	104.2	40.1
5	20	324	92.3	33.5		50	89.8	32.1
5	5	156	93.8	34.3		30	90.4	32.4
7	20	187	93.8	34.3		22	105.4	40.8
7	14	219	89.0	31.7		8	93.0	33.9
9	20	326	90.0	32.2	3	76	98.2	36.8
9	9	248	92.8	33.8		69	93.0	33.9
10	20	239	89.5	31.9		20	88.6	31.4
12	20	259	87.0	30.6	7	93	99.8	37.7
12	5	115	88.0	31.1	6	60	103.2	39.6
14	20	374	93.3	34.1	4	80	84.6	29.2
14	6	55	90.8	32.7	3	60	106.2	41.2
16	20	186	92.3	33.5	4	45	92.0	33.3
					_			
AVERAG	Ε	197	91.0	32.8	3	85	94.7	34.8
No. Ma for T	neuvers WD	36				72		
Avg. T	WD/Maneuver	5.5			5	.3		

TABLE VII

TEST VEHICLE VAPOR LOCK AND CITY DRIVEABILITY RANKINGS

	City	(.	0242	
Rank	Driveabili TWD	Car No.	Critical T _{V/L=20} @ 95°F (35°C	C) Car No.
1	0	8	<103 (<39.4)	3
2	9	6	<108 (<42.2)	2
3	22	7	<108 (<42.2)	13
4	24	13	<111 (<43.9)	18
5	60	11	<113 (<45.0)	8
6	61	18	107 (41.7)	6
7	70	19	111 (43.9)	17
8	99	2	113 (45.0)	4
9	138	17	113 (45.0)	7
10	164	3	119 (48.3)	9
11	214	15	121 (49.4)	15
12	376	9	122 (50.0)	11
13	445	16	124 (51.1)	10
14	480	14	124 (51.1)	14
15	772	10	125 (51.7)	12
16	775	1	126 (52.2)	5
17	812	12	127 (52.8)	16
18	850	5	127 (52.8)	19
19	891	4	>150 (>65.5)	1

TABLE VIII

CARBURETOR FUEL LINE TEMPERATURES FOR 95°F(35°C) VAPOR LOCK TESTS

Car No.	Critical Vapor Lock Condition (1)	Temperatu Key-Off Ambient	res, °F Soak Carb.	<u> </u>	Temperatu Idle S Ambient		<u>∆</u> (2)
1	I	105	150	45	104	180(183)(3)	76
3	NL	102	173	71	107	172(176)	65
4	KO	88	147(147)	59	87	144	57
5	I	92	194	102	90	194(188)	104
6	I	102	188	86	104	180(179)	76
7	I	105	170(170)	65	105	170	65
9	I	106	156	50	100	167(170)	67
10	I	97	147	50	97	156(152)	59
11	KO	89	193	104	~-		
12	I	111	174	63	102	176(184)	74
13	NL	110	160	50	102	153(161)	51
14	I	110	216	106	101	183(194)	82
15	I	97	168	71	95	173(173)	78
16	I	101	152	51	94	156(160)	62
17	I	90	130	40	90	134	44
18	NL	89	151	62	90	124	34
19	I	107	172	65	91	160(168)	69

⁽¹⁾ I = Idle, NL = Not Limited, KO = Key-Off.

⁽²⁾ \triangle = Carburetor Temperature - Ambient Temperature.

⁽³⁾ Number in parentheses is the average temperature for only those runs in which both key-off and idle soaks were conducted.

TABLE IX

CARBURETOR FUEL LINE TEMPERATURES FOR 70°F(21°C) VAPOR LOCK TESTS

Car No.	Critical Vapor Lock Condition(1)	Temperatu Key-Off Ambient		<u> </u>	Temperatu Idle S Ambient	ires, °F Soak Carb.	<u>∆</u> (2)
1	ко	75	129	54	76	159	83
3	NL	78	145	67	80	142	62
4	I	76	138	62	77	135	58
5	I	75	173	98	78	171	93
6	КО	77	158	81	78	159	81
7	ко	73	142	69	74	139	65
9	КО	77	140	63	77	127	50
10	ко	76	131	55	77	136	59
11	КО	77	185	108	77	148	71
12	I	74	147	73	77	156(152)(3)	79
14	I	75	184(177)	109	74	164(156)	90
15	NL	65	136	71	66	139	73
16	I	81	136	55	74	131(148)	57
17	NL	-			79	114	35
19	I	76	148	72	77	145	68

⁽¹⁾ I = Idle, NL = Not Limited, KO = Key-Off.

⁽²⁾ \triangle = Carburetor Temperature - Ambient Temperature.

⁽³⁾ Number in parentheses is the average temperature for only those runs in which both key-off and idle soaks were conducted.

TABLE X

FUEL PUMP INLET AND FUEL TANK TEMPERATURES FOR 95°F(35°C) VAPOR LOCK TESTS

C	Critical		eratures				eratures,	°F	
Car No.	Vapor Lock Condition (1)	Amb.	y-Off So Pump	ak Tank	<u>∆</u> (2)	Amb.	Idle Soak Pump	Tank	<u>^</u> (2)
1	I	105		110	5	104		113(112)(3)	9
3	NL	102		106	4	107		116(118)	9
4	KO	88	128		40	87	128		41
5	I	92				88		97	9
6	I	102		108	6	104		111(112)	7
7	I	105		108(10	8) 3	105		114	9
9	I	106	144		38	100	148(152)		48
10	I	97	125		28	97	147(144)		50
11	KO	92	142(153)	50	106	174		68
12	I	111	125		14	102	151(158)		49
14	I	110	172		62	101	151(194)		50
15	I	97		113	16	97		113(110)	16
16	I	101	154		53	94	161(164)		67
19	I					89	168		79

⁽¹⁾ I = Idle, NL = Not Limited, KO = Key-Off.

⁽²⁾ Δ = Fuel Pump Inlet or Fuel Tank Temperature - Ambient Temperature.

⁽³⁾ Number in parentheses is the average temperature for only those runs in which both key-off and idle soaks were conducted.

TABLE XI

FUEL PUMP INLET AND FUEL TANK TEMPERATURES FOR 70°F(21°C) VAPOR LOCK TESTS

Car	Critical Temperatures, °F Vapor Lock, Key-Off Soak					Temperatures, Idle Soak			
No.	Condition (1)	Amb.		Tank	_Δ (2)	Ать.	Pump	Tank	<u>Δ</u> (2)
1	КО	75		82	7	76		87	11
3	NL	78		82	4	80		91	11
4	1	76	119		43	77	118		41
5	I	75		80(83)(3)	5	78		88	12
6	KO	77		83	6	78		87	9
7	КО	73		80	7	74		86	12
9	КО	77	120		43	77	119	~-	42
10	ко	76	108		32	77	123		46
11	ко	76	126		50	76	145		69
12	I	74	98		24	77	134(120)		57
14	I	75	140(133)		65	74	125(120)		51
16	I	81	137		56	74	136(155)		62
19	I	76	111		35	77	148		71

⁽¹⁾ I = Idle, NL = Not Limited, KO = Key-Off.

⁽²⁾ Δ = Fuel Pump Inlet or Fuel Tank Temperature - Ambient Temperature.

⁽³⁾ Number in parentheses is the average temperature for only those runs in which both key-off and idle soaks were conducted.

TABLE XII

CONDITION OF MAXIMUM TEMPERATURE VERSUS VAPOR LOCK CRITICAL CONDITION

	95°F	(35°C) Vape	or Lock	70°F (21.C) Vapor Lock			
Car	Critical Vapor Lock	Condition Temperatu	n for Highest ure Recorded	Critical Vapor Lock	Condition Temperat	on for Highest cure Recorded	
No.	Condition	Carb.	Fuel Pump	Condition	Carb.	Fuel Pump	
1	I	I	••	KO	I		
3	NL	I		NL	KO		
4	КО	KO	KO & I	I	ко	КО	
5	I	KO		I	KO	KO	
6	I	KO		KO	I		
7	I	KO & I	•-	KO	KO		
9	I	I	I	KO	ко	KO	
10	I	I	I	K0	I	I	
11	КО		I	KO	KO	I	
12	I	I	I	I	I	I	
13	NL	I					
14	I	KO	I	I	KO	KO	
15	I	I		NL	I		
16	I	I	I	I	I	I	
17	I	I		NL		I	
18	NL	KO		I	KO	I	
19	I	KO		I	KO	I	

NOTE: I = Idle; NL = Not Limited; KO = Key Off

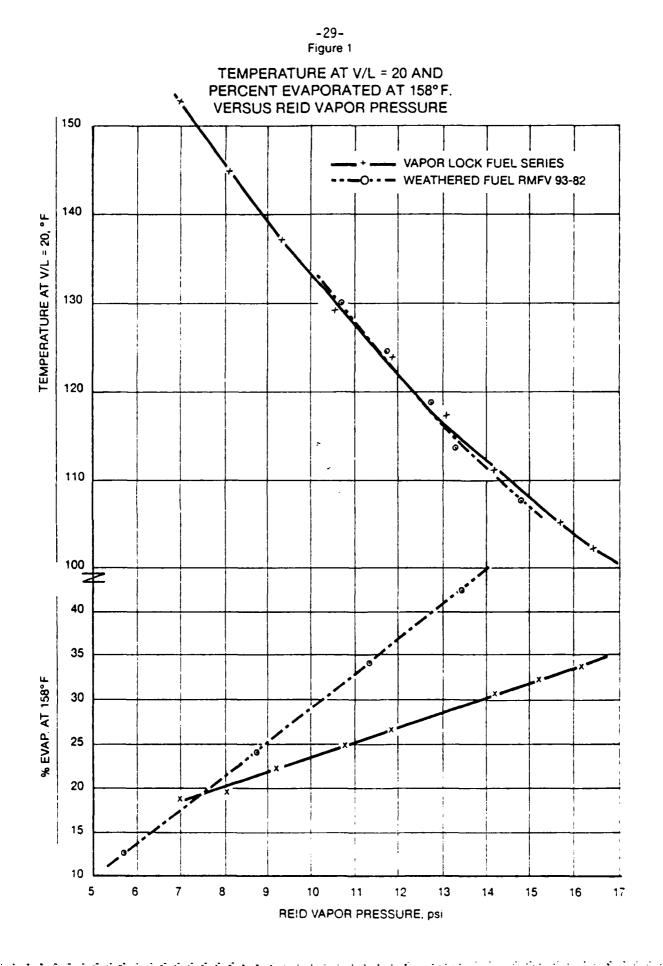
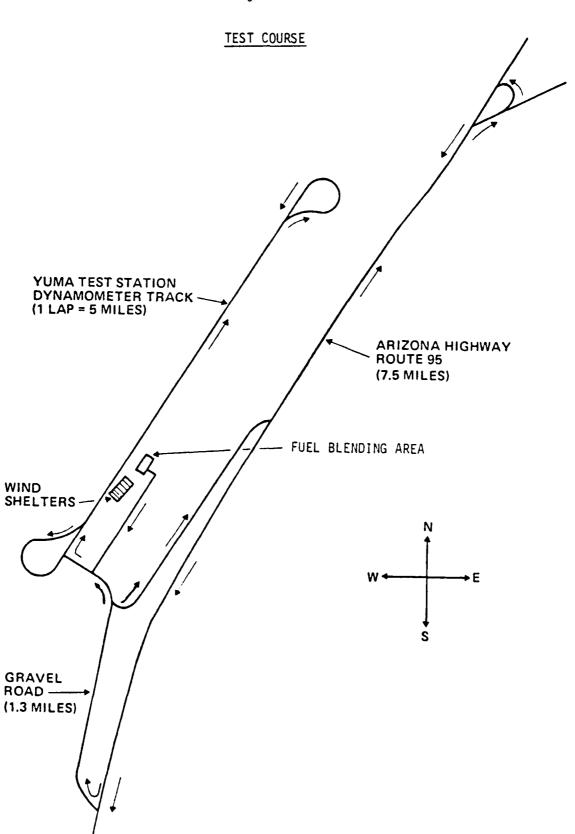
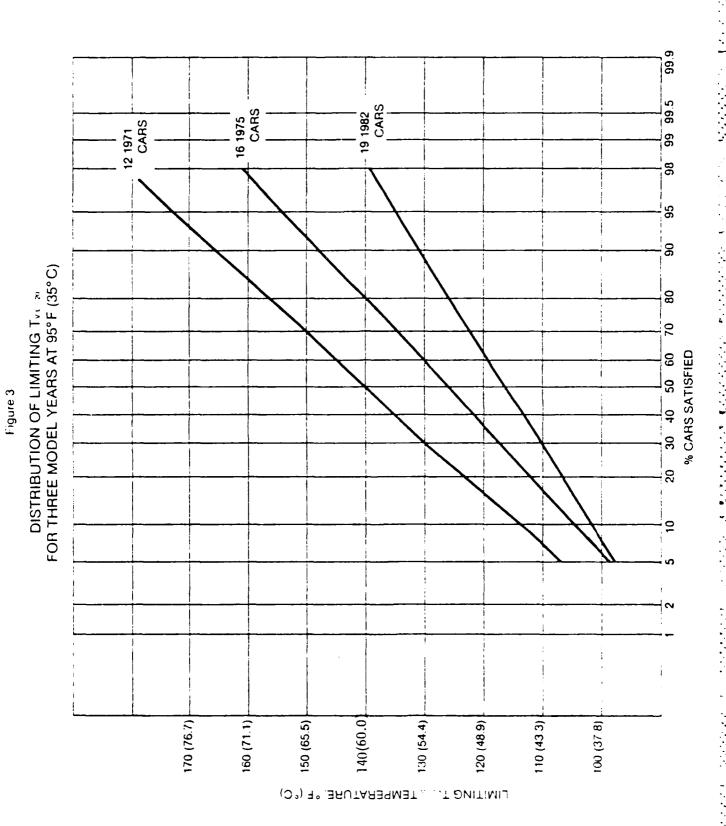


Figure 2



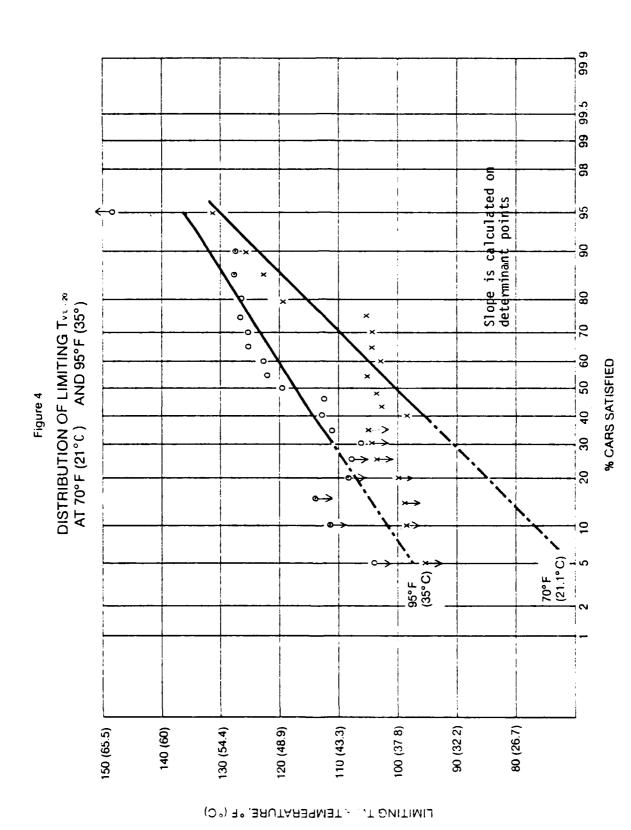


▶ ストラスのの名間 ののそののの名間のようななのの●

ストランスの ● とうかなかなが、●こうななななが、●

シスクス 日子と子がなりと

■ からから、 A Min のでは、 ■ 大学のでは、 ● からでは、 1



FUEL-RETURN LINE -- NON-FUEL-RETURN LINE Slope is calculated determinant points DISTRIBUTION OF LIMITING Tw.:»
OF 1982 MODEL YEAR CARS
EQUIPPED WITH FUEL-RETURN VERSUS NON-FUEL-RETURN LINES Figure 5 140 (60) 150 (65.5) 130 (54.4) 120 (48.9) 110 (43.3) 100 (37.8)

LIMITING TAL- TEMPERATURE, °F (°C)

% CARS SATISFIED

99.9

99.5

66

8

50 60

30, 40

20

Figure 6
TWD's: COMPARABLE DRIVEABILITY RUNS

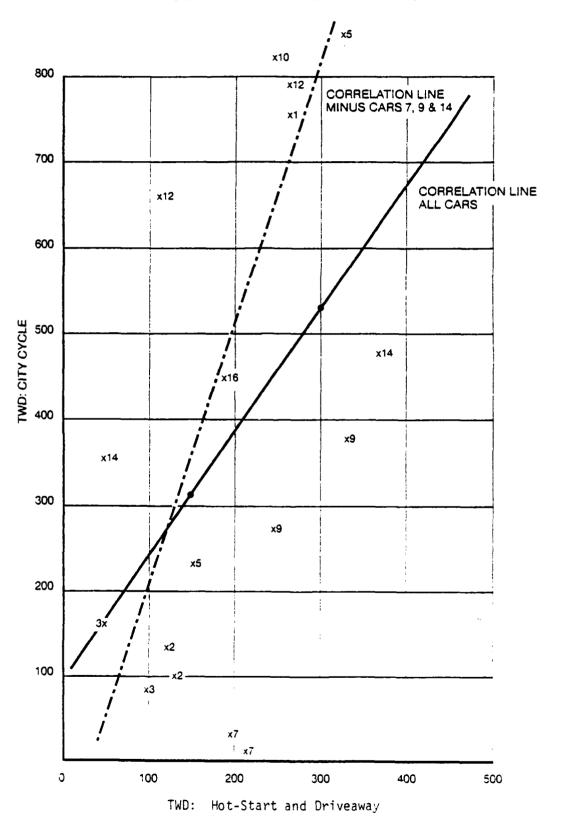
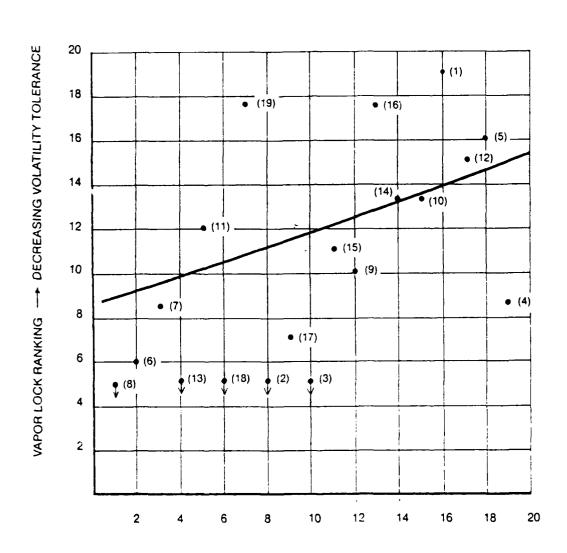


Figure 7

VEHICLE RANKING:

VAPOR LOCK VERSUS HOT START AND DRIVEAWAY

(BY CAR NUMBER)



HS&D RANKING → INCREASING TWD (CITY DRIVEABILITY TEST — FUEL RMFV 93-82)

APPENDIX A

PROGRAM PARTICIPANTS
AND
PANEL MEMBERSHIPS

PROGRAM PANEL

Name Company J. E. Robinson, Ldr. J. C. Ingamells D. K. Lawrence R. E. Paggi R. L. Russell E. H. Schanerberger R. T. Simmons M. S. Stawnychy E. D. Steinke Company Standard Oil Company (Ohio) Chevron Research Company Amoco Oil Company Texaco Inc. Union Oil Company of California Ford Motor Company Chrysler Corporation Mobil Research & Development Corp. Sun Tech, Inc.

ANALYSIS PANEL

Name	Company
J. E. Robinson, Ldr.	Standard Oil Company (Ohio)
D. A. Barker	Shell Development Company
K. D. Eng	Texaco Inc.
J. L. Keller	Consultant
P. D. McFarland	Amoco Oil Company
R. L. Russell	Union Oil Company of California
M. S. Stawnychy	Mobil Research & Development Corp.
F. D. Steinke	Sun Tech. Inc

PROGRAM PARTICIPANTS

	Name	Company
D. <i>A</i>	A. Barker	Shell Development Company
A. E	E. Buczynsky	Sun Tech, Inc.
). Esau	Amoco Oil Company
	N. Hall	Chevron Research Company
	S. Hyek	Gulf Research & Development Company
	. Keller	Consultant
	4. Mathis	American Honda
	McDonald	Carter Automobile Div., ACF Industries
	E. McCorkell	Union Oil Company of California
	. Ness	Phillips Petroleum Company
	Noquehi	American Honda
	E. Robinson	Standard Oil Company (Ohio)
	M. Reuter	Texaco Inc.
	. Russell	Union Oil Company of California
	Shaw	Carter Automobile Div., ACF Industries
	Smith	Southwest Research Institute
	S. Stawnychy	Mobil Research & Development Corp.
	D. Steinke	Sun Tech. Inc.
	Toshimitsu	American Honda
	Tsukamoto	American Honda

APPENDIX B

PROGRAM: 1982 CRC HIGH-TEMPERATURE

DRIVEABILITY PROGRAM

1982 CRC HIGH-TEMPERATURE DRIVEABILITY PROGRAM CRC Project No. CM-118-82

Prepared by the

Program Panel

of the

CRC Light-Duty Volatility Group

February 1982

Revised: May 1982

1982 CRC HIGH-TEMPERATURE DRIVEABILITY PROGRAM

Objective

Determine vapor lock performance of a selected group of 1982 cars at nominal temperature of 70°F and 95°F. Determine hot start and drive-away performance of the same group of cars at a nominal temperature of 95°F.

Introduction

CRC has conducted high temperature programs for the evaluation of vapor lock and hot start and driveability on 1972 and 1975 model passenger cars. Since 1975, changes in vehicle design that may affect high temperature performance are exhaust emission systems, design for fuel economy, and introduction of new front wheel drive designs. This program will indicate the effect of such changes on vapor lock performance at a nominal temperature of 95°F. In addition, vapor lock will be evaluated at a nominal temperature of 70°F. The lower temperature vapor lock evaluation will be useful in updating ambient temperature corrections of volatility and in giving guidance for volatility specification for a range of temperatures from 70 to 95°F.

A new hot start and driveaway procedure will be investigated in this program. The new procedure emphasizes conditions that might cause performance problems encountered in heavy stop and go traffic after a period of temperature stabilization. Selected cars will compare performance results from the 1975 CRC hot start and driveaway procedure to the new procedure.

Test Fuels

Vapor lock test fuels consisting of three base fuels of 6.0, 12.0, and 17.0 RVP are identified as RMFV 90-82, 91-82, and 92-82, respectively. The fuel series is representative of a typical 10.5 lb. RVP summer fuel and a 13.5 lb. RVP winter fuel. Test fuel specifications are shown in Attachment A.

A special fuel blended to emphasize hot start and driveaway problems is also shown on the fuel specification sheet as RMFV 93-82. Use of this fuel is discussed in the test procedure section.

Test Cars

Twenty-one test vehicles are selected for the test program as follows for 1982:

Car No.		Make and Model	Engine Size, Liter/Type
1	GM T	Body Chevrolet Chevette Pontiac T-1000	1.6/L-4
2	GM J	Body Chevrolet Cavalier Pontiac J-2000 Buick Skyhawk Oldsmobile Firenza Cadillac Cimmaron	1.8/L-4
3	GM A	Body Chevrolet Celebrity Pontiac A-6000 Buick Century Oldsmobile Ciera	2.5/L-4
4	GM X	Body Chevrolet Citation Pontiac Phoenix Buick Skylark Oldsmobile Omega	2.8/٧-6
5	GM G	Body Chevrolet Malibu Chevrolet Monte Carlo Pontiac Bonneville Pontiac Grand Prix Buick Regal Oldsmobile Cutlass	2.8/V-6
6	GM G	Body Chevrolet Malibu Chevrolet Monte Carlo Pontiac Bonneville Pontiac Grand Prix Buick Regal Oldsmobile Cutlass	3.0/٧-6
7		Buick Regal	3.8/V-6
8		Buick LeSabre	4.1/V-6
9	Ford	Escort-Mercury Lynx	1.6/L-4
10	Ford	Mustang-Mercury Capri	2.3/L-4
11	Ford	Futura-Granada	3.3/L-6

Car No.	Make and Model	Engine Size, Liter/Type
12	Ford Futura-Granada	3.8/٧-6
13	Ford Futura-LTD-Thunderbird	4.2/٧-8
14	Plymouth Reliant-Dodge Aries	2.2/L-4
15	Datsun 210	1.4 or 1.5/L-4
16	Toyota Corolla	1.8/L-4
17	Volkswagen Rabbit	1.6/L-4
18	Honda Accord	1.8/L-4
19	Chevrolet Van	5.0/٧-8
20	Ford Van	4.9/V-8
21	Dodge Van	3.7/L-6

In some cases, several vehicles are listed, such as Chevrolet Celebrity, Pontiac A-6000, Oldsmobile Ciera, or Buick Century for a General Motors A-body car with a 2.5-liter engine. The actual car to be tested will be determined by a particular model of the choices listed being available from the rental agency. If one or more of the selected vehicles are not available, alternate selections are as follows:

- 1. Dodge Diplomat, or equivalent, with a 3.7-liter engine
- 2. Cadillac Deville with a 4.1-liter engine
- 3. Lincoln with a 5.0-liter engine
- 4. Chevrolet S-10 pickup truck
- 5. Ford Ranger pickup truck with a 2.3-liter engine

All vehicles are to be equipped with automatic transmission and air conditioning. Car preparation will include checking timing, idle speed, emission control system operation, installation of vacuum gauge lines, installation of temperature thermistors and installation of fuel tank drains.

Vapor Lock Test Procedure

The vapor lock test procedure will essentially be the same as used in the 1975 CRC program. A copy of this procedure is shown as Attachment B. Sections 12a, b, c, d, and e will change the speed for determining increases in acceleration times from 70 mph to 60 mph. Test temperatures will be 65 to 80°F for the lower temperature portion of the program and 90 to 105°F for the higher temperature portion. Data will be corrected to 70 and 95°F for the lower and higher temperatures of the program.

If time allows, selected cars will be evaluated by an alternate vapor lock procedure. Vapor lock evaluation will be made by timing accelerations from 0 to 30, 50, and 60 mph. All other aspects of the alternate procedure will be the same as the CRC procedure. Purpose is to compare the severity of timed accelerations from 0 to 30, 50, and 60 mph of the alternate procedure with timed accelerations of 15 to 50, 60, and 70 mph of the current CRC procedure.

Hot Start and Driveaway Test Procedure

The hot start and driveaway test procedure is designed to appraise low speed driveability and hot starting problems. The procedure is based on a similar procedure devised and conducted by Amoco Oil Company. The procedure consists of stabilization at 55 mph, simulated city traffic for 4 miles to maximize engine heating, a 10 minute idle soak, simulated city traffic for 3 miles, a 20 minute key-off soak, and simulated city traffic for 3 miles. Details of the procedure are included as Attachment C. Stabilization will be run on the highway and the simulated city course in a marked course on the Yuma Proving Grounds Dynamometer Track.

Each car will make the following runs:

- two fuels bracketing the critical vapor lock fuel (\pm 1 lb. RVP)
- duplicate tesets with Fuel RMFV 93-82
- the lowest volatility fuel (6 lb. RVP) only if problems occur with Fuel RMFV 93-82.

Fuel RMFV 93-82 is a high volatility, pentane-rich fuel that is designed to emphasize problems occurring in simulated low speed city driving. Fuel samples will be obtained at the end of each soak and inspected for RVP using an automatic RVP apparatus.

If time allows, up to five selected cars that had hot start and driveaway problems on the new procedure will also be run on the 1975 CRC Hot Start and Driveability Procedure. This will allow comparison of the severity of the two procedures. The 1975 CRC Hot Start and Driveability Procedure is included as Attachment D.

Temperature Measurements

Temperature measurements will be obtained at two locations on all vehicles. A common point of temperature measurement will be the surface temperature of the vehicles fuel line at a position of 6 to 12 inches from the carburetor. The second temperature point will be selected by the various car manufacturers or by panel members if a recommendation is not made by the manufacturers. Temperatures will be obtained during the first and last minute of all soak periods for vapor lock and hot start and driveaway tests.

Test Location and Schedule

Suitable temperatures and facilities are available at the Yuma Army Proving Grounds. Suggested timing is September 20, 1982 to October Twenty-three test days are available. Two days are rescheduled for test site setup and driver practice. Temperature studies indicate a daily average of 2.2 hours of 70 to 80°F temperatures, and 5.1 hours of 90 to 100°F temperatures. Additional test time is probably available because of extending the test temperatures to 65 to 80°F and 90 to 105°F. With three-man test crews a full vapor lock test requires 55 minutes. After establishing the most severe soak, idle or key off, a vapor lock test requires 35 minutes. With the assumption that three vapor lock tests (one out of three to be a full vapor lock test) can be averaged for the 2.2 hours available at the lower temperatures and six at the higher temperatures, it will require 14 test days to complete the 65 to 80°F vapor lock tests and 7 days to complete the 90 to 105°F vapor lock tests. The hot start and driveaway tests will require 12 days to complete at 90 to 100°F. This leaves an allowance of 7 days at the lower temperature and 2 days at the higher temperature for adverse weather or alternate vapor lock procedure.

Manpower

Manpower requirements are based on a four-week test program, twentyone test vehicles, and three test crews. Requirements are as follows:

- 3 Drivers-Raters
- 3 Observers
- 3 Preparers and Warmup
- 1 Data Analysis
- 1 Lab Operator
- I Track Boss
- 1 Track Assistant and Fuel Dispenser

¹³ Total

TEST FUEL SPECIFICATIONS FOR 1982 VOLATILITY PROGRAM

	RMFV 90-82(1) <u>RMFV 91-82</u>	RMFV 92-82 ⁽²⁾	RMFV 93-82
RVP, psi	6.0 ± 0.5	12.0 ± 0.5	17.0 ± 0.5	13.5 ± 1
Distillation, °F (D86)				
10% Evap.	145 ± 10	110 ± 10	90 ± 10	95 ± 10
30% Evap.	200 ± 10	160 ± 10	140 ± 10	135 ± 10
50% Evap.	235 ± 10	215 ± 10	205 ± 10	175 ± 10
70% Evap.	270 ± 10	265 ± 10	260 ± 10	230 ± 10
90% Evap.	350 ± 10	345 ± 10	345 ± 10	290 ± 10
End Point	437 Max.	437 Max.	437 Max.	437 Max.
Percent Evap. @ 158°F				40 - 45
<u>V/L 20, °F</u>				108 ± 4
<u>Octane</u>				
MON		85 Min.		
(R+M)/2		89 Min.		
Lead, g/gal		0.05 Max.		
Phosphorus, g/gal	ı	0.005 Max.		
Sulfur, % wt.		0.10 Max.		
Benzene, % vol.		1.0 Max.		
Antioxidant, PTB Phenylene Diamine type		5 Min.		

^{(1) 10.5} psiRVP blend of RMFV 90-82 and RMFV 91-82 to have percent evap. @ 158°F between 25-30%.

^{(2) 13.5} psiRVP blend of RMFV 91-82 and 92-82 to have percent evap. @ 158° F between 30-35%.

ATTACHMENT B

CRC VAPOR LOCK TEST PROCEDURE

- 1. Drain gasoline tank and refill with 8 gallons (6 gallons with tanks of 16-gallon capacity or less) of test fuel for the next test. Test fuel shall not be put in tanks more than 10 minutes before the start of the test. Take fill sample in duplicate if scheduled.
- 2. Drive 20 miles at 55 mph for vehicle warm-up, establishing base total start time after 15 miles of operation.
- 3. Obtain baseline acceleration time on the track following 15 miles of warm up by accelerating from a stop, at light throttle, to reach 10 mph within 5 seconds. Then accelerate at the desired throttle position (wide-open throttle) to 70 mph, timing by stopwatch from 15 mph to 50, 60, and 70 mph, as indicated by speedometer. Record acceleration times and note surging or abnormal vehicle performance. Complete one lap around the track at 55 mph and return to wind shelter.
- 4. Park car in soak shed for 15 minutes with engine off. Obtain soak fuel sample in duplicate.
- 5. At end of soak period, start car using vehicle manufacturer's recommended procedure. Record start time to nearest 0.1 second and number of stalls. Idle for 5 seconds in neutral after the original start and any restarts, and record any abnormality in the stability of idle performance. Accelerate from soak shed as described in Item 6.
- 6. Turn headlights on. Obtain wide-open throttle acceleration time by accelerating from the soak shed at part throttle to reach 10 mph in 5 seconds, and then accelerate at wide-open throttle to 80 mph, recording time from 15 mph to 50, 60, and 70 mph. Record acceleration time and abnormal vehicle performance. In this technique, a transient and/or abnormal change in acceleration rate is called surge. The intensity of surge may vary, as described below:

<u>Satisfactory (S)</u> - A rating indicating no malfunction. Some loss in acceleration may be measured, but no surging in the accepted understanding of the term may be recognized.

Trace (T) - A rating that is just discernible to a test driver; or might not be observed by the casual driver.

Moderate (M) - A rating that is judged to be probably noticeable to the average driver and definitely noticeable to the test driver. It is occasional in frequency and is associated with limited delays in acceleration rather than an actual decrease in speed.

Heavy (H) - A rating that is pronounced and judged to be obvious to any driver. It is persistent or constant in frequency and is associated with prolonged delays in acceleration or even actual decreases in speed level reached.

<u>Lock (L)</u> - That which completely stalls the engine over a stretch of at least 3/10 of a mile, or a period of time in excess of 20 seconds.

Turn headlights off at north turn.

- 7. Complete two laps around the track at 55 mph, to restabilize temperatures.
- 8. Idle for 10 minutes in neutral in the soak shed. Record number of stalls. Obtain "idle" fuel sample in duplicate.
- At end of idle period, accelerate from soak shelter as described in Item 6.
- Complete one lap around the track at 55 mph; return to fueling area.
- 11. Car volatility tolerances are to be defined only for the more critical condition (soak or idle); the remaining tests will be run as follows:
 - a. If the fuel selected for the previous test was either too volatile or too low in volatility to determine whether the idle or the soak acceleration was the more critical, the soak and idle procedure shall be repeated on a new test fuel.
 - b. If, during the preceding test, the soak acceleration is found to be appreciably more critical than the idle acceleration (>20% increase in acceleration time) with a fuel giving 25 to 75% loss in acceleration performance, the remaining tests will be run using only the soak procedure, otherwise the idle procedure will be used in all cases.
- 12. Continue testing with other fuels of different T-V/L levels to obtain curves of acceleration time from 15-50, 15-60, and 15-70 mph versus fuel volatility. To establish the vehicle limiting T-V/L data, a minimum of five fuels of each series will be tested at the desired limiting condition (soak or idle). Fuels will be selected with the following objectives:
 - a. A fuel with sufficient volatility to cause acceleration time to 70 mph to increase between 50 and 100%.
 - b. A fuel with sufficient volatility to cause acceleration time to 70 mph to increase between 25 and 50%.

- c. A fuel with sufficient volatility to cause acceleration time to 70 mph to increase between 10 and 25%.
- d. A fuel with sufficient volatility to result in less than a 10% increase in acceleration time, or if minimum acceleration time exceeds 10%, two fuels giving essentially equal performance and differing by at least 4°F in the temperature for 20:1 V/L ratio (0.5 to 1.0 lb RVP).
- e. A fuel estimated to give a 25% increase in acceleration time to 70 mph.

ATTACHMENT C

CITY DRIVEABILITY PROCEDURE

AND DRIVEABILITY RATINGS

- Stabilize engine and fuel system temperatures by driving 15 miles at 55 mph.
- 2. Drive 4 miles in "city" traffic simulated as follows:
 - A. Within each mile stop 4 times for a 15 second idle, and at the end of each mile idle for 30 seconds to record driveability problems. All idle soaks should be about 0.2 miles apart.
 - B. Maximum car speed should be 20 mph.
 - C. Accelerate very gently following each idle by dropping the engine vacuum at the start of an acceleration by 5" Hg below its idle value and hold the throttle at this position until the car reaches 20 mph.

The purpose of this portion of the test is to maximize engine heating and underhood temperatures. During this portion of the test, the driver should rate the severity of subjective problems, such as hesitation, stumble, surge, idle roughness, and backfire; and count the number of stalls.

- 3. Idle for 10 minutes in the soak shelter with the transmission in neutral or "Park" for safety. Appraise idle quality, record stalls and restart times if stalling occurs. Obtain fuel samples for RVP inspection.
- 4. Leave the soak shelter and make a 0-30 mph part-throttle (3" Hg manifold vacuum) acceleration. Observe severity of any acceleration problems including hesitation, stumble, and surge.
- 5. Drive 3 miles in city traffic per Step 2 above.
- Park in a soak shelter for 20 minutes with key off. Observe hot start stalls and measure restart time. Obtain fuel samples for RVP inspection.
- 7. Repeat Step 4 above.
- 8. Compile driveability demerits for the cycle using an appropriate rating scale, which weighs problems according to their relative severity.

ATTACHMENT D

CRC HOT START AND DRIVEAWAY PROCEDURE

- 1. Drain fuel tank and fill with 8 gallons of test fuel.
- 2. Drive 20 miles at 55 mph for vehicle warm-up, establishing base total start time after running 15 miles of operation.
- 3. Pull into soak shed and idle in neutral for 10 minutes. Record idle speed and quality initially, after 5 minutes, and at the end of 10 minutes.
- 4. Back vehicle out of soak shed for approximately 30 feet and stop abruptly (10 ft./sec.²). Record idle quality during 10-second idle in drive. Also number of stalls, and restart time, if any.
- 5. Accelerate from 0 to 30 mph at 5 ft./sec.², stop abruptly (20 ft./sec.²). Evaluate and record hesitation, stumble, surge, and stall.
- 6. Idle in drive for 15 seconds, recording idle quality.
- 7. Accelerate at 5 ft./sec.² from 0-45 mph. Evaluate and record hesitation, stumble, surge, and stall.
- 8. Make four successive accelerations from 0-25 mph at 5 ft./sec.². Decelerate moderately, using brake, and idle for 15 seconds following each acceleration. Record hesitation, stumble, surge, stall, and idle speed and quality for each cyclo of operation.
- 9. Immediately following final 15 second idle in Item 8, accelerate at 8" Hg. constant manifold vacuum from 0-55 mph. Record hesitation, stumble, surge, and stalls.
- 10. Complete 10 miles at 55 mph for temperature restabilization.
- 11. Pull into soak shed and idle in drive for one minute. Record idle speed and quality.
- 12. Turn off engine and soak for 20 minutes. Obtain duplicate fuel sample.
- 13. At the end of the soak period, with the transmission in park or neutral, set the throttle to manufacturer's recommendation. Engage the starter immediately after opening throttle. Do not pump the throttle before making the start. If the engine does not start after 15 seconds of cranking, depress throttle to floor board; crank an additional 15 seconds to check for overrich condition. If engine does not start, manipulate throttle as required to start engine. Record initial start time and detail any abnormal starting procedure.

- 14. When engine starts, allow it to accelerate to 1000 rpm before deenergizing start motor and releasing throttle to idle position. The engine must continue to run for one minute after the throttle is returned to idle to constitute a successful start and run test. If engine stalls, immediately repeat starting and idle procedure. If engine stalls 4 times in succession, increase idle speed as required to keep engine running. Evaluate and record idle quality and speed, number of stalls, and total starting time. Total starting time is the cumulative period of time the starter motor is engaged. The time interval that the engine is idling between stalls is not included in total starting time.
- 15. Repeat Items 4 through 9 and return to fueling area.

APPENDIX C

FUEL INSPECTION DATA

1982 CRC HIGH-TEMPERATURE DRIVEABILITY PROGRAM

Fuel 1

	Ľa	Lab. 1	Lab.	2	Lab.	3	Lab.	4		
		2	-	2		2		2	Avg.	Std. Dev.
RVP, psi	7.4	7.0	7.0	7.0 7.0	7.0	7.0	7.3	7.0	7.1	0.16
API Gravity	57.0	57.0	56.9	56.8	56.7	57.0	56.5	56.3	56.8	0.26
T _{V/L=20} , °F	154	154	153.1	153.0	154.3	154.3 153.4	149.0	149.0 149.0	152.5	2.19
Distillation (D86) T°F @ % Evap.										
IBP	108	101	93	66	94	96	87	88	96	6.9
5	130	127	123	122	120	114	113	114	120	6.3
10	142	140	138	138	138	130	131	134	136	4.3
20	165	163	191	161	162	154	157	159	160	3.5
30	188	187	187	186	187	181	183	184	185	2.4
40	212	209	210	211	210	205	206	206	209	2.6
20	231	229	229	230	230	225	227	227	228	2.0
09	248	247	247	248	249	243	245	244	246	2.1
70	269	268	271	271	289	265	566	265	270	7.8
80	303	300	304	303	308	300	300	299	302	3.0
06	348	345	352	348	349	343	345	347	347	2.8
95	375	373	384	378	381	374	374	376	377	3.9
EP	417	415	410	408	412	414	430	432	417	0.6

1982 CRC HIGH-TEMPERATURE DRIVEABILITY PROGRAM

Fuel 3

	Lab	Lab. 1		2	Lab.	3	Lab.	4		
	1	2		2		2		2	Avg.	0 21
RVP, ps i	7.6	8.2		8.1	8.1	8.1	8.5	8.5	8.2	
API Gravity	57.8	57.8		57.7	57.7	57.5	57.4	57.6	57.6	
$^{\mathrm{T}}_{\mathrm{V/L=20}}$ °F	148	146		145.1 145.1	146.0	146.0 146.8	141.4	141.4 141.5	145.0	2.37
Distillation (D86) T°F @ % Evap.										
IBP	96	100	93	93	96	26	88	92	94	3.4
2	118	122	118	114	115	119	114	114	117	3.0
10	132	136	132	130	132	134	131	129	132	2.2
20	156	159	157	155	158	159	159	157	158	1.5
30	182	185	184	182	184	185	185	183	184	1.3
40	205	208	208	208	209	208	210	208	208	1.4
50	226	229	229	230	231	229	233	228	229	2.1
09	244	247	247	248	248	248	250	247	247	1.7
70	792	569	270	569	272	272	271	268	270	2.1
80	299	302	303	301	305	304	304	301	302	2.0
06	346	347	350	347	347	346	352	348	348	2.1
95	373	375	379	378	378	375	377	375	376	2.1
EP	414	418	410	412	413	416	432	428	418	7.9

1982 CRC HIGH-TEMPERATURE DRIVEABILITY PROGRAM

Fuel 5

	•1						C	-3										
	St	.27	.14	1.40		3.2	6.1	3.9	3.3	3.3	2.8	2.2	3.0	1.7	2.1	2.9	3.8	8.9
,	Avg.	9.3	58.5	137.2		88	107	123	148	177	203	225	244	266	300	345	376	416
4	7	7.6	58.4	135.1		82	107	122	148	171	203	223	243	266	298	345	374	422
Lab.	- -	7.6	58.4	134.9		83	102	119	146	176	202	224	237	265	300	345	374	424
		9.3				98	100	118	144	171	198	222	242	264	297	341	373	408
Lab. 3	2	9.3	58.7	137.0		88	101	120	144	173	200	223	243	265	298	342	373	410
	-	9.4	58.3	138.0		88	105	125	151	179	205	226	246	569	303	347	381	414
2	2	9.3	58.6	137.0		88	107	123	147	176	204	225	244	267	299	345	377	408
Lab. 2	-	9.3 9.3	58.6	138.6		93	113	127	151	179	205	226	245	268	302	351	384	414
. 1	2	0.6	58.5 58.5	138		92	117	129	153	182	207	229	247	268	302	347	375	418
Lab. 1	-	8.9	58.5	138		06	114	127	151	178	204	227	246	266	301	344	375	426
		RVP, psi	API Gravity	TV/L=20' °F	Distillation (D86) T °F @ % Evap.	IBP	5	10	20	30	40	20	09	70	80	06	95	EP

1932 CRC HIGH-TEMPERATURE DRIVEABILITY PROGRAM

Fuel 7

	Lab. 1	. 1	Lab. 2	2 2	Lab.	Lab. 3	Lab. 4	4 2	Avg.	Std. Dev.	
RVP, ps i	10.2	10.3	10.6	10.7	10.6	10.5	11.1	10.6	10.6	0.27	
API Gravity	58.8	59.7	59.5	59.6	59.4	59.2	59.5	59.5	59.4	0.28	
^r V/L=20°°F	132	130	130.0	129.3	129.3	129.3	125.3	126.7	129.0	2.08	
Distillation (D86) T°F @ & Evap.											
	93	90	91	98	88	84	88	88	88	2.8	
	108	109	104	102	101	101	100	111	104	4.2	
	120	121	118	116	119	118	115	133	120	5.6	
	144	146	143	140	144	144	142	150	144	2.9	
	174	175	173	170	173	171	170	171	172	1.9	
	202	203	201	199	202	198	198	198	200	2.1	
	225	226	225	223	225	221	221	224	224	1.9	
	244	245	244	243	245	242	243	240	243	1.7	
	264	265	366	264	267	265	592	268	597	1.4	
	297	297	300	297	299	298	302	305	299	2.9	
	342	343	349	343	341	342	352	353	346	4.9	
	370	372	377	371	373	375	386	392	377	7.9	
	418	417	408	408	416	405	432	434	417	10.8	

1982 CRC HIGH-TEMPERATURE DRIVEABILITY PROGRAM INDIVIDUAL LABORATORY RESULTS

Ω,
7
ë
Œ

	Lab.	. 1	Lab.	2	Lab.	m	Lab.	4		
	-	2		2		2		2	Avg.	Std. Dev.
RVP, psi	11.5	11.5	11.7	11.7	11.8	11.8	12.3	12.3	11.8	0.32
API Gravity	60.5	60.7	60.3	60.4	60.2	60.4	60.1	60.2	60.4	0.19
TV/L=20' °F	122	125	127.0	127.0 121.5	124.7	124.7 122.7	120.4	120.4 120.4	123.0	2.38
Distillation (D86) T°F @ & Evap.										
IBP	87	87	93	88	98	83	82	85	98	3.4
2	103	102	102	100	86	96	96	96	66	3.0
10	117	114	116	114	115	112	113	112	114	1.8
20	138	138	138	137	140	137	137	137	138	1.0
30	167	168	169	166	171	166	168	167	168	1.7
40	197	197	199	198	201	198	197	197	198	1.4
50	222	222	222	221	226	222	221	221	222	1.6
09	242	242	242	241	246	243	243	242	243	1.5
70	263	263	267	265	268	764	265	264	265	1.8
80	295	295	298	297	300	298	297	298	297	1.7
06	341	342	349	346	345	341	344	344	344	2.7
95	372	370	387	380	377	373	377	377	377	5.3
EP	415	414	408	406	416	414	427	432	416	8.8

1982 CRC HIGH-TEMPERATURE DRIVEABILITY PROGRAM

Fuel 11

×	۱ ۵.	_	_														
Std. De	0.32	0.5(2.67		3.9	6.0	2.9	3,3	3.2	2.4	2.1	4.4	3.2	3,3	2.9	4.8	9.6
Avg.	13.1	61.4	116.5		81	91	106	131	161	193	220	239	263	296	343	376	416
4 2	13.6 13.6	61.0	113.6		78	98	104	132	163	194	221	243	267	297	346	380	432
Lab	13.6	9.09	113.4		92	84	103	134	163	194	219	241	3 66	298	344	377	428
3	13.2 13.1	62.2	117.3		79	88	105	129	161	193	219	239	265	298	345	381	413
Lab.	13.2	61.1	114.9		81	92	109	134	166	198	224	245	267	301	347	382	414
2 2	12.9 12.9	61.3	115.4		79	84	102	124	155	189	217	238	259	291	340	371	403
Lab.	12.9	61.2	117.5		98	95	108	130	160	193	219	239	262	294	343	379	408
Lab. 1	12.9	61.8	121		98	66	109	133	161	193	219	230	260	294	341	370	415
Lab	12.8	61.6	119		82	97	109	132	162	193	220	240	261	293	339	372	415
	RVP, psi	API Gravity	TV/L=20"°F	Distillation (D86) T°F@&Evap.	IBP	S	10	20	30	40	20	09	70	80	06	95	EP

1982 CRC HIGH-TEMPERATURE DRIVEABILITY PROGRAM INDIVIDUAL LABORATORY RESULTS

Fuel 13

	Lab.	1 2	Lab. 2 1 2	2 2	Lab.	Lab. 3	Lab.	Lab. 4	Avg.	Std. Dev.
RVP, psi	13.9	14.1	14.0	14.1	14.3	14.3	14.5	14.7	14.2	0.27
API Gravity	62.4	62.8	62.1	62.3	62.2	62.2	61.8	61.2	62.1	0.47
TV/L=20°°F	110	115	110.0	109.5	110.3	109.9	109.0	109.0	110.3	1.94
Distillation (D86) T°F @ % Evap.										
IBP	87	84	88	84	9/	79	7.7	75	81	5.1
2	95	91	90	1	81	84	ı	ı	88	5.6
10	105	102	105	86	66	103	90	96	100	5.1
20	126	123	127	124	125	129	117	121	124	3.7
30	155	153	158	152	156	159	147	152	154	3.8
40	188	187	192	187	188	190	180	187	187	3.5
50	216	215	220	217	218	219	208	216	216	3.7
09	238	238	240	238	241	242	231	239	238	3.3
70	259	257	262	258	260	262	254	263	259	3.0
80	291	291	296	292	294	295	286	300	293	4.2
06	341	339	351	344	342	344	341	354	344	5.3
95	369	369	383	ı	373	375	ı	1	374	5.8
ďa	415	415	406	408	413	412	421	425	414	6.3

1982 CRC HIGH-TEMPERATURE DRIVEABILITY PROGRAM

Fuel 15

	Lab.	. 1	Lab.	7	Lab.	m	Lab.	4		
	-	2		2		2		2	Avg.	Std. Dev.
RVP, psi	15.2	15.1	15.2	15.4	15.3	15.4	15.5	15.9	15.4	0.25
API Gravity	63.4	63.1	63.1	63.3	62.8	63.0	62.6	62.5	63.0	0.32
T _{V/L=20} °F	110	112	104.6	104.6 104.6	105.3	105.3 105.3	104.6	104.6 104.3	106.3	2.95
Distillation (D86) T°F@ & Evap.										
IBP	80	80	82	75	9/	80	72	9/	78	3.4
2	84	98	ı	ı	11	83	ı	1	82	3.9
10	98	86	96	98	06	86	94	94	94	4.3
20	119	119	121	114	105	122	122	124	118	6.1
30	149	148	151	143	134	152	155	157	149	7.3
40	184	183	187	180	171	185	189	190	184	6.0
50	214	213	216	209	202	215	216	217	213	5.0
09	236	235	238	231	226	240	236	239	235	4.6
70	257	256	260	255	248	260	259	264	257	4.7
80	290	286	292	285	283	293	300	301	291	6.7
06	349	334	356	343	335	340	355	355	346	9.1
95	361	379	1	1	366	371	1	ı	369	7.7
EP	415	414	399	401	408	413	434	428	414	12.1

1982 CRC HIGH-TEMPERATURE DRIVEABILITY PROGRAM

Fuel 17

	<u>י</u>	Tab. 1		,	J.	٠-	[ab.	7		
		2		1 2		2		2	Avg.	Std. Dev.
RVP, psi	16.1	16.2		16.5	16.6	16.4	16.2	16.2	16.3	0.18
API Gravity	64.3	64.4		64.0	63.8	63.4	63.5	63.5	63.8	0.38
TV/L=20'°F	110	110		99.4	100.1	100.1 102.4	98.2	98.2 98.2	102.2	5.02
Distillation (D86) T°F 0 % Evap.										
IBP	92	84	79	77	80	78	75	92	78	2.9
Z.	ı	ı	1	ı	ı	ı	ı	t	ı	ı
10	92	95	06	ı	93	96	1	ı	93	2.4
20	113	115	115	108	115	118	105	107	112	4.7
30	142	143	145	136	144	149	135	139	142	4.7
40	179	179	184	176	180	187	174	177	180	4.2
20	211	211	214	208	213	218	207	210	212	3.5
09	234	234	236	231	238	241	231	236	235	3.4
70	256	255	261	255	261	265	253	257	258	4.0
80	286	286	292	285	293	300	282	290	289	5.7
06	335	335	349	339	344	354	1	ı	343	7.8
95	1	1	ı	1	1	ı	ı	1	,	i
EP	414	413	399	412	418	420	418	421	414	7.0

1982 CRC HIGH-TEMPERATURE DRIVEABILITY PROGRAM

Fuel 20

	Lab.	. 1	Lab.	Lab. 2	Lab.	2	Lab.	4	į	, rod
	-	7	-	7	1	7	4	7	Avg.	sed. Dev.
RVP, psi	13.3	13.3	13.6	13.8	13.9	13.8	12.8	12.8	13.4	0.44
API Gravity	74.8	74.8	74.4	74.4	74.0	74.1	74.3	74.1	74.4	0.31
$T_{V/L=20}'$ °F	108	107	106.9	107.1	107.8	107.8 107.8	106.7	106.7 106.4	107.2	0.58
Distillation (D86) T °F @ % Evap.										
IBP	79	80	79	81	80	76	80	78	79	1.6
5	89	93	85	06	06	98	90	87	68	2.6
10	96	66	86	86	101	97	86	96	86	1.6
20	105	111	109	109	115	110	111	111	110	2.8
30	121	127	124	124	131	126	130	127	126	3.3
40	143	149	152	147	154	151	151	150	150	3.4
50	178	182	183	182	190	187	184	184	184	3.6
09	216	219	211	216	221	219	216	215	217	3.1
70	231	231	232	234	237	235	236	234	234	2.2
80	243	244	248	246	254	252	255	252	249	4.6
06	287	293	302	296	306	306	312	300	300	8.0
95	346	351	361	348	355	354	364	361	355	6.5
EP	409	407	410	408	414	409	432	428	415	8.6

APPENDIX D

TEST PROCEDURES
AND
DATA RATING SYSTEMS

I. TEST PROCEDURES

A. CRC Vapor Lock Test Technique

- Drain gasoline tank and refill with six gallons of test fuel for the next test. Test fuel shall not be put in tanks more than 10 minutes before the start of the test.
- 2. Drive 20 miles at 55 mph for vehicle warm-up, establishing base total start time after 15 miles of operation.
- 3. Obtain baseline acceleration time on the track following 15 miles of warm up by accelerating from a stop, at light throttle, to reach 10 mph within 5 seconds. Then accelerate at the desired throttle position (wide-open throttle) to 70 mph, timing by stopwatch from 15 mph to 50, 60, and 70 mph, as indicated by speedometer. Record acceleration times and note surging or abnormal vehicle performance. Complete one lap around the track at 55 mph and return to wind shelter.
- 4. Park car in soak shed for 15 minutes with engine off. Obtain soak fuel sample in duplicate.
- 5. At end of soak period, start car using vehicle manufacturer's recommended procedure. Record start time to nearest 0.1 second and number of stalls. Idle for 5 seconds in neutral after the original start and any restarts, and record any abnormality in the stability of idle performance. Accelerate from soak shed as described in Item 6.
- 6. Turn headlights on. Obtain wide-open throttle acceleration time by accelerating from the soak shed at part throttle to reach 10 mph in 5 seconds, and then accelerate at wide-open throttle to 70 mph, recording time from 15 mph to 50, 60, and 70 mph. Record acceleration time and abnormal vehicle performance. In this technique, a transient and/or abnormal change in acceleration rate is called surge. The intensity of surge may vary, as described below:

Satisfactory (S) - A rating indicating no malfunction. Some loss in acceleration may be measured, but no surging in the accepted understanding of the term may be recognized.

<u>Trace (T)</u> - A rating that is just discernible to a test driver, or might not be observed by the casual driver.

Moderate (M) - A rating that is judged to be probably noticeable to the average driver and definitely noticeable to the test driver. It is occasional in frequency and is associated with limited delays in acceleration rather than an actual decrease in speed.

Heavy (H) - A rating that is pronounced and judged to be obvious to any driver. It is persistent or constant in frequency and is associated with prolonged delays in acceleration or even actual decreases in speed level reached.

 $\underline{\text{Lock (L)}}$ - That which completely stalls the engine over a stretch of at least 3/10 of a mile, or a period of time in excess of 20 seconds.

- 7. Complete two laps around the track at 60 mph, to restabilize temperatures.
- 8. Idle for 10 minutes in neutral in the soak shed. Record number of stalls. Obtain "idle" fuel sample in duplicate.
- 9. At end of idle period, accelerate from soak shelter as described in Item 6.
- 10. Complete one lap around the track at 60 mph, and return to fueling area.
- 11. Car volatility tolerances are to be defined only for the more critical condition (soak or idle); the remaining tests will be run as follows:
 - a. If the fuel selected for the previous test was either too volatile or too low in volatility to determine whether the idle or the soak acceleration was the more critical, the soak and idle procedure shall be repeated on a new test fuel.
 - b. If, during the preceding test, the soak acceleration is found to be appreciably more critical than the idle acceleration (>20% increase in acceleration time) with a fuel giving 25 to 75% loss in acceleration performance, the remaining tests will be run using only the soak procedures; otherwise the idle procedure will be used in all cases.
- 12. Continue testing with other fuels of different T-V/L levels to obtain curves of acceleration time from 15-50, 15-60, and 15-70 mph versus fuel volatility. To establish the vehicle limiting T-V/L data, a minimum of five fuels will be tested at the desired limiting condition (soak or idle). Fuels will be selected with the following objectives:
 - a. A fuel with sufficient volatility to cause acceleration time to 70 mph to increase between 50 and 100%.
 - b. A fuel with sufficient volatility to cause acceleration time to 70 mph to increase between 25 and 50%.

- c. A fuel with sufficient volatility to cause acceleration time to 70 mph to increase between 10 and 25%.
- d. A fuel with sufficient volatility to result in less than a 10% increase in acceleration time; or if minimum acceleration time exceeds 10%, two fuels giving essentially equal performance and differing by at least 4°F in the temperature for 20:1 V/L ratio (0.5 to 1.0 lb RVP).
- A fuel estimated to give a 25% increase in acceleration time to 70 mph.

B. CRC Hot Start and Driveaway Test Technique

- 1. Drain fuel tank and fill with six gallons of test fuel.
- 2. Drive 20 miles at 55 mph for vehicle warm-up, establishing base total start time after running 15 miles of operation.
- 3. Pull into soak shed and idle in neutral for 10 minutes. Record idle speed and quality initially, after 5 minutes, and at the end of 10 minutes.
- 4. Back vehicle out of soak shed for approximately 30 feet and stop abruptly (10 ft./sec.2). Record idle quality during 10-second idle in drive. Also record the number of stalls, and restart time, if any.
- 5. Accelerate from 0 to 30 mph at 5 ft./sec.², and stop abruptly (20 ft./sec.²). Evaluate and record hesitation, stumble, surge, and stall.
- 6. Idle in drive for 15 seconds, recording idle quality.
- 7. Accelerate at 5 ft./sec.² from 0-45 mph. Evaluate and record hesitation, stumble, surge, and stall.
- 8. Make four successive accelerations from 0-25 mph at 5 ft./sec.². Decelerate moderately, using brake, and idle for 15 seconds following each acceleration. Record hesitation, stumble, surge, stall, and idle speed and quality for each cycle of operation.
- 9. Immediately following the final 15-second idle in Item 8, accelerate at 8" Hg constant manifold vacuum from 0-55 mph. Record hesitation, stumble, surge, and stalls.
- 10. Complete 10 miles at 55 mph for temperature restabilization.
- 11. Pull into soak shed and idle in drive for one minute. Record idle speed and quality.

- 12. Turn off engine and soak for 20 minutes. Obtain duplicate fuel sample.
- 13. At the end of the soak period, with the transmission in park or neutral, set the throttle to manufacturer's recommendation. Engage the starter immediately after opening throttle. Do not pump the throttle before making the start. If the engine does not start after 15 seconds of cranking, depress throttle to floor board; crank an additional 15 seconds to check for overrich condition. If engine does not start, manipulate throttle as required to start engine. Record initial start time and detail any abnormal starting procedure.
- 14. When engine starts, allow it to accelerate to 1000 rpm before de-energizing start motor and releasing throttle to idle position. The engine must continue to run for one minute after the throttle is returned to idle to constitute a successful start and run test. If engine stalls, immediately repeat starting and idle procedure. If engine stalls four times in succession, increase idle speed as required to keep engine running. Evaluate and record idle quality and speed, number of stalls, and total starting time. Total starting time is the cumulative period of time the starter motor is engaged. The time interval that the engine is idling between stalls is not included in total starting time.
- 15. Repeat Items 4 through 9 and return to fueling area.

C. City Driveability Procedure

- 1. Stabilize engine and fuel system temperatures by driving 15 miles at 55 mph.
- 2. Drive 4 miles in "city" traffic, simulated as follows:
 - a. Within each mile, stop 4 times for a 15-second idle, and at the end of each mile, idle for 30 seconds to record driveability problems. All idle soaks should be about 0.2 miles apart.
 - b. Maximum car speed should be 20 mph.
 - c. Accelerate very gently following each idle by dropping the engine vacuum at the start of an acceleration by 5" Hg below its idle value and hold the throttle at this position until the car reaches 20 mph.

The purpose of this portion of the test is to maximize engine heating and underhood temperatures. During this portion of the test, the driver should rate the severity of subjective problems, such as hesitation, stumble, surge, idle roughness, and backfire; and count the number of stalls.

- 3. Idle for 10 minutes in the soak shelter with the transmission in neutral or "Park" for safety. Appraise idle quality, record stalls and restart times if stalling occurs. Obtain fuel samples for RVP inspection.
- 4. Leave the soak shelter and make a 0-30 mph part-throttle (3" Hg manifold vacuum) acceleration. Observe severity of any acceleration problems including hesitation, stumble, and surge.
- 5. Drive 3 miles in city traffic per Step 2 above.
- 6. Park in a soak shelter for 20 minutes with key off. Observe hot start stalls and measure restart time. Obtain fuel samples for RVP inspection.
- 7. Repeat Step 4 above.
- 8. Compile driveability demerits for the cycle using an appropriate rating scale which weights problems according to their relative severity.

II. DATA RATING SYSTEMS

A. Vapor Lock Rating System

Reid vapor pressures measured on samples from the car tank for each road test were converted to equivalent $T_{V/L=20}$ based on the correlation established in Section IV. These values were then adjusted for the difference between ambient air temperature at the time of testing and the reference temperature of 95°F or 70°F as follows:

Adjusted
$$T_{V/L=20}$$
 = Actual $T_{VL=20}$ + K (or - Air T)
(70)

Printouts of complete vapor lock data for each car are presented in Appendix G. Because surge was encountered in many of the base accelerations*, average base acceleration times were taken from those accelerations judged to best represent base-line performance.

^{*} The frequency of surge in base accelerations in this program may be related to the slight delay at the end of the warm-up run needed to stop and allow the test crew to replace the warm-up driver.

Adjusted temperatures at V/L=20 were plotted against percent increase in car acceleration time at 15-50 mph, 15-60 mph, and 15-70 mph for all test sets. From these plots the most critical speed range and the limiting temperature at V/L=20 (hereafter described as $\rm LT_{V/L=20}$) were determined for 25% as in previous programs*.

B. Driveability Demerit Rating System

Starting Time - Time recorded in seconds (hot-start time is the sum of times for initial start and all restarts).

Stalls at Idle - Number of occurrences during each maneuver or time period.

Stalls, Driving - Number of occurrences during each maneuver.

Weighted demerits are assigned to each malfunction as summarized below:

Weighted Demerits**

Starting time:	Seconds - 2.0	0
-	(but zero if nega	ative)
Stalls at idle:	8	
Stalls, driving:	32	
•	T M	<u>H</u>
Idle roughness	1 2	4
Backfire	6 12	24
Hesitation	6 12	24
Stumble	6 12	24
Surge	4 8	16

The total weighted demerit (TWD) value for each run was computed by adding the weighted demerits for the several malfunctions in each maneuver or idling period, subject to the following constraints:

^{*} For example, reference, "1966 CRC Vapor Lock Tests," CRC Report No. 420.

^{** &}quot;Evaluation of a High Temperature Driveability Test Procedure - 1971 Yuma Program," CRC Report No. 455.

- 1. Only one driving stall was counted per maneuver.
- No more than three idling stalls were counted per idling interval.
- 3. No more than five idling stalls were counted for the whole hot-start and idle procedure (lines 14-18 of data sheet).
- 4. For each maneuver or idling interval, only the one malfunction giving the highest weighted demerits was counted. Thus, if heavy hesitation (24 weighted demerits) and a stall were recorded in the same maneuver, only 32 weighted demerits were counted towards the TWD.

Start End	ACCELERATION TIME, sec	15 mph	
Time, Base Run: Odometer, Base Run: Time, Key-Off Soak: Time, Idle Soak:	STARTING		
tn Car end:	UEATUED	· udm	
Car Make: Run No. (Office Use Observer: Gal: A:		Start Just of Before Soak Acceler- ation Air:	Air: Air:
Car No.: Date: Driver No.: Fuel No.: Temperature Probe at:	COMMENTS:	SAMPLE NUMBERS BASE RUN	101 ING SOAK

		i					D-1	_	
	End							sec.	00 dm 09
	ابد							ACCELERATION TIME,	- hqm 0 50 mph
	Start							ACCEI	0 mph-30 mph
OCK DAIA SHEET		Time, Base Run:	Odometer, Base Run:	Time, Key-Off Soak:	Time, Idle Soak:			STARTING	Time, — — Sec. — — — — — — — — — — — — — — — — — — —
1982 CRC ALIERNAIE VAPUR LUCK DAIA SHEEI		•	No. in Car Odor	Blend: Time	Blend: Time	B:		i 1	Sky Cover: Shade:N,P,S Wind from mph. Wind from - N,NE,E,etc.
_	Car Make:	_ Run No. (Office Use)	Observer:	Gal:	Gal:	A:		TEMPERATURES	Start Just of Before Soak Acceler- ation
	Car No.:	Date:	Driver No.:	Fuel No.:		Temperature Probe at:	COMMENTS:	SAMPLE	BASE RUN

D-10 1975 CRC TRAFFIC DRIVEAWAY DATA SHEET

Run No.:	Date:
Car No.:	Fuel No.:
Driver:	Observer:
Sample No.; End of Test	

		·Ne							Idle			D	ri.	rin	<u>.</u>
Line No.	Mođe	Instruc.	Time of Day	Ambient Temp.	Overheat	Packfi re	Starting Time; Sec.	RPM	Range	Roughness	Stalls	tion		Surge	
1	Base Start Time	5													. لنت
3	E o Initial														
3	Initial Journal 10 min.	3													
4															
5	Back-Up & Stop	11													
6	Accel 0-30 & st Accel 0-45		l												;
7		7	•		igsqcut		i				_			_	1
9	Accel <u>0-25</u>					-					_		_		_[:
9	<u>0-25</u>	3									_¦			_	
10	<u>0-25</u> 0-25			j		\dashv	į				_				∤.
12	Accel 0-60	Q,					Į						-		:
	Idle Drive	17	1				1								. لــــ
	Hot Start	13				_		·		╁╼╁					
				•				· · · · · · · · · · · · · · · · · · ·							
15 16 17 18	in.	14													
17	l min. idle								****						
18	<u>ч</u>														
19	Back-Up & Stop	_4							`].
20	400el Q=30 % s	5/6					[
1 1	Accel 0-45	7					,								
22	Accel <u>0-25</u>						ļ				_				
23	0-25 0-25 0-25 0-25	3				_	ļ				- 1	_			
24	0-25				_	_	}					_	_		:
25	0-25					_	Į					_		_	_ :
	Aggel 0-60 COMMENTS:	C	1								ŧ				

					<u>.</u> . <u>.</u>		1	٦					į	D- '	11																					
11	Ϋ́I		,	į	Park, 20 min.]	A	A	3.8	\Box	-]	-	-					-	-	-	i		١٠		_		!			_	٢	\neg	7	٦
9	In. Pa			Ì	ċ	[1	7	Ĩ.		3.6		_	_						_	-	_	min.		ole r's	_	-	res,	cf Park	-	-	-	Park	-	-	-
Time & Odometer @Start of:	20 min. Brk			į	ldle, 10 min.	L					3.4		_		-								Park 20 m	PT Accel.	Park Sample	-	-	emperatures						<u>-</u> -		_
@S1	14/6	}	1		.5=		1 1	ר			. 2		7	_	_						_		-Park	- PT /	Pari	لـــ		Tem	Start	Air:	¥.	.; ;;	End of	Air:	.: ¥	.: ::
ter-	10-mm. 141e	Ì		WEATHER -	Start, 0.0 mi	L		_			.0*		-	-						_	_				ا ـــــا	<u>-</u> -1							i	<u>.</u>	` - T	_
lome	اء اء	1 	1	. WEAT		<u>:</u>	ند و				e,	3	-	-	-					-	_	-		*	70.		-	-	-			1		- -	- -	
\$ 00	First Idle					Sky (SN, SC, CL, OV)	Wind velocity, mph:	Mind From (N,ME,E,etc			2.8		-	-	-					-	1	-	†	A	6.8		-	-	-		1	_	\dashv	-	-	-
me	First			ļ	•	SC, (city	5			5.6		_	_	_ -					_	_	-			9.9		_	_	_	İ	-		_	_	_	_
1	·		<u>:</u>			(SN,	yeld	5			2.4		\dashv					1 (1						-	4.0	•			_	- 5		1		1	_	_
		Time:	Odometer	i 		Sky	Wind				2		_	_	_					_	_				6.2			_					-	\exists	4	4
i		Ξ.	8								7 2.		-		_					-	_	-	*						_			j		-	1	_
	1								sec/30 sec at	10115	2,0	H	-	-	-	201				-	-	-	sec/30 sec at	IONS	6 .0 ,		-	-	-		-		\dashv	-	-	-
1	ا اخ	ا							/30 s	ACCELERATIONS	1.8		-	-	_					-	_	-	/30 \$	LERAT	رم ج		-	-	-		1	-		-	-	-]
	Blend:	Blend:			•				s sec,	ACCE	9.1		_	_	_					_	_		5 sec	GENTLE ACCELERATIONS	5.6			_	_			1	_	_	_	_
							•		ES, 15	GENTLF	₹.		-					2.0	pla 2		_		10LES, 15	ENTLE	ارم ت-	-					-+	- (+	\dashv	\dashv
Fuel No:	ا <u>:-</u>	_ <u></u>							- IDLES,	9	.2		_	_	_				_		- -	_	151		2 5	_	-	-	_					- - 	\dashv	4
F.	Ga 1:	Gal:									-		-	-	-		- T		1111	_	_	-			لئ		-	_	-			1		-		
											1.0		-]	-	-					-	-	-			5.0		-	-	-		-		_	-	-	-
											0.8		_	_	_					_	_	-			₹.		_	-	_		-1			- -	_	_
		in Car:	Ì								9.0		_					-	-	H		-	$\ $		9.4									_	_	_
İ	,		1							İ	4		_	_					18.5	_	_	-	$\left\{ \left[\right] \right\}$	ļ	4									-	$\frac{1}{1}$	\exists
		Š	ä								2 0.		-	_	_	_				_	_	-			¥.		-	_	-			्रं		-	_	
		Ì									.0		-	-	-	-	_	_	- 0	-	-	-	*	٧	4.2	-	-	-						-	-	_
	fice)								+	A	0		_] /	,	, O		_	-	-			 		-	-	_
	. (of	er:									st:	اسا		sec	<u>. </u>	يسل	<u> </u>	<u> </u>	l	·	<u> </u>] : L	(i	Sec	L	ا ـــا ع	1	<u> </u>				 ~_
Car Make:	Run No. (Office):	Observer:	ا تخ								Mile Post:	Roughness	Stalls, #	Restarts, sec	Problem X	Hesitation	Chumble	a 9	our ye Rackfiro	Stalls	Dynchlem Y	Problem Z	Idle 10 min:	PI Accel:	Hile Post	Roughness	Stalls, #	Restarts, sec	Problem X	Hesitation	Stumble	e E	Sackfire	Stalls, A	Problem 1	Problem Z
C	œ	0	•								Ξ	Rou	Sta		Pro	100			Surge Backfi	2 2		P - 0	:	<u> </u>	Ξ	Rouc	Stal	Res	l Prot	Hes	Stul	Surge	280	<u>\$</u>	Pre	Pro
}	1												370					1011	- EBA	UEI	ΩA				v		31	9			,		l∀d.	1 11.) A	
			s at	ي: ا										ature	Idle	-	-	-							le #	-	-	s a	dle	-	-	-	6	-	-	-
ë	Ì	Driver No:	Temp Probes at	COMMENTS:										Temperatures,	First Idle										Idle Sample #'s	-	-	Temperatures.	of Idle	L	_	Ľ.	i Idle	_	_	
Car No:	Date:	Orive	Temp	ප								-		<u>_</u>		A1r:		: 32	;						Idle	_	-] dui.4]	Start	Air:	A:	.: ::	End of	Air:	A:	 øa
_	_	_							•																					-					•	

APPENDIX E

RATER COMPARISONS

CITY DRIVEABILITY PROCEDURE

APPENDIX E

RATER COMPARISONS - CITY DRIVEABILITY PROCEDURE

Past programs have shown large differences can exist among raters when evaluating vehicle driveability. To evaluate rater differences, data on cars driven by the same rater on the same fuels provide the best measures of biases. Ratings were obtained by each rater on the same fuel (No. 20) for only two vehicles:

Vehicle	Rater 04	Rater 10	Rater 17	Average	St. Dev.	St. Dev.
10	917	874,766	530	755.7	201.4	27
12	884	793,761	812	824.3	54.6	7

^{*}Standard deviation as percent of the mean.

Because of the inconsistencies indicated above and the small amount of data, rater severity values could not be developed to correct the TWD values for each vehicle/fuel combination.

Repeatability can best be measured by comparison tests performed by individual raters on the same vehicle/fuel combinations. Repeat ratings were completed by Rater 04 with three vehicles and by Rater 10 with two vehicles:

Rater	Car	<u>Fue1</u>	Run 1	Run 2	Average	St. Dev.	St. Dev., %
04	9 14 14	1 1 20	184 112 393	269 48 567	226.5 80.0 480.0	60.1 45.3 23.0	26.5 56.6 25.6 Avg. = 36.2
10	10 12	20 20	874 793	766 761	820.0 777.0	76.4 22.6	9.3 2.9 Avg. = 6.1

Rater 04 may have had difficulty repeating ratings, or the particular cars Rater 04 ran for repeatability were not consistent in driveability. No repeatability data were available for Rater 17.

APPENDIX F

EFFECTS OF FUEL VOLATILITY CHANGES
CITY DRIVEABILITY PROCEDURE

APPENDIX F

EFFECTS OF FUEL VOLATILITY CHANGES - CITY DRIVEABILITY PROCEDURE

Total weighted demerit values obtained with the nineteen test fuels are shown in Table F-1 and illustrated in Figure F-1. As indicated, all vehicles were tested on at least two fuels, and every vehicle was tested on Fuel 20. As time permitted, vehicles with high demerit levels with Fuel 20 were tested using the vapor lock fuels. The test plan called for each car to run two vapor lock fuels bracketing the critical fuel. Because bracketing fuels varied for the different vehicles, an unbalanced data set was created, causing significant difficulty in model development.

Initially, to determine if changes in fuel volatility significantly affected TWD ratings, the data for vehicles tested on the extreme fuels were averaged and compared. In this data set, seven vehicles were tested on two fuels of widely different volatility (Vehicles 1, 4, 6, 9, 10, 12, and 14 on Fuels 1 and 20). Although these data are limited, the average TWD values follow the expected trend, increasing considerably as fuel volatility increases:

	Avg. TWD fcr		nspections	
Fuel No.	Seven Vehicles	RVP, psi	T_V/L=20	<u>% 158</u>
1	219	7.1	152.5	19.2
20	552	13.4	107.2	42.4

The analysis was expanded to include data for all fuels and all vehicles, rater biases, car biases, and ambient temperature. Ambient temperature was found to be insignificant in the temperature range tested and was excluded from further model development. The expanded model, excluding ambient temperature, was:

TWD =
$$b_0 + b_1 C_1 + b_2 C_2 + ... + b_{19} C_{19} + b_{20} R_{04}$$

+ $b_{21} R_{10} + b_{22} R_{17} + b_{23} T_{V/L=20}$
+ $b_{24} \%158 + b_{25} RVP$

where:

C = dummy variable for Cars 1-19R = dummy variable for Raters 04, 10, 17

The three fuel variables did not appear to be significant, indicating the combination of variables did not correlate with TWD. Rater coefficients were insignificant; therefore, the rater effect was eliminated from further model development. Correlation and regression coefficients are shown in Table F-II.

Fuel variables were next examined individually. The models used were developed using the common log of the TWD values. A constant of 10 was added to the TWD term to raise it above zero.

Models used for separately correlating RVP, %158, and $T_{V/L=20}$ were:

RVP:

Log (TWD + 10) =
$$b_1 C_1 + b_2 C_2 + ... + b_{19} C_{19} + b_{25} (RVP - 12.4)$$

%158:

Log (TWD + 10) =
$$b_1 c_1 + b_2 c_2 + ... + b_{19} c_{19} + b_{24} (\%158 - 33.7)$$

$$T_{V/L=20}$$
: Log (TWD + 10) = $b_1 C_1 + b_2 C_2 + ... + b_{19} C_{19} + b_{23} (T_{V/L=20} - 120.3)$

Results follow the expected trend -- TWD values increase as fuel volatility increases. All three fuel variables appear to be equally good predictors of hot-weather driveability and not just $T_{V/L}=20$, as for the 1975 CRC program. When using individual fuel variables, the model correlation coefficients improved. Correlation and regression coefficients are shown in Table F-II.

TABLE F-I

DRIVEABILITY RESULTS - CITY PROCEDURE

50	775 99 164 891*	F-3 0 0 0 0 0	376/81 917/874/766/530* 60 884/793/761/812*	$\frac{24}{393/567}$ $\frac{214}{445*}$	$124/151*$ $\frac{61}{70}*$
17	126 86 942*	110 40 1		101	179
14		88 I			
13			254	;;;;	
11 erits			!!!!		; ; ; ; ; ;
10 11				804	
9 10 11 Total Weichted Demerits	232		184/269 727 		
æ			578		
9			1111	360	
S		530	099	44*	÷29
ო	394		1 48		111
1	757	105	246 116 	112/48	
Fue]:					
	Car 1 2 3	8 7 6 5	9 10 11 12	13 14 15 16	17 18 19

04 - No additional marking 10 - Underlined 17 - Asterisked ** Rater indicated by:

TABLE F-11

REGRESSION EQUATIONS - IND AS A FUNCTION OF FUEL PROPERTIES

				A	egression	Regression Coefficient	=			
Equation Form	PO	-	<u></u>	[P	$-b_0$, b_1 , $-b_2$, $-b_3$, b_4 , $-b_5$, $-b_6$, $-b_1$, $-b_0$, $-b_1$	9q	by	84	ęd .
IMD = b ₀ + b ₁ -19 ^C 1-19 + 8 ₂₀₋₂₂ R + · b ₂₃ T _{V/L=20} + b ₂₄ \$158 + b ₂₅ RVP	3385.7	0.0	-749.2	-448.4	173.6	3385.7 0.0 -749.2 -448.4 <u>173.6 -241.0</u> -689.0 -581.0 -613.4	0.689-	-541.0	-613.4	-49R.R
log(1Mb+10) = b1-19 C1-19 + b23 (1y/L=20-120.3)	;	2.1		1.9 2.1	2.7	2.3	1.9	1.4	1.4 1.0	2.4
log(IWD+10) = b ₁₋₁₉ C ₁₋₁₉ + b ₂₄ (X158-33.7)	;	2.7		2.0 2.1 2.7	2.7	2.1		 5.	1.9 1.5 1.0	7.4
log(TWD:10) * b1-19 Cj-19 + b25 (RVP-12.4)	;	1.3		1.9 2.1 2.7	2.7	2.1		7:	1.9 1.4 1.0 2.4	7.4

NOTE: Underlined coefficients are not significant at 95% confidence.

TABLE F-11

REGRESSION EQUATIONS - TWO AS A FUNCTION OF FUEL PROPERTIES

					Regression Coefficient	Coefficie	nt			
Equation Form	<u>6</u> 10-	<u>-11</u>	<u>-</u> 21 <u>-</u>	blobloblobloblo	-b14-	-\$1 4	<u>-614</u> <u>-615</u> <u>-616</u> <u>-617</u>	-11 -	61 4 81 4	61 <u>q</u>
$1MD = b_0 + b_{1-19} C_{1-19} + B_{20-22} R + b_{23} I_{V/L=20} + b_{24} x_{158} + b_{25} RVP$	27.5	-733.9	83.7		-742.3 -368.8 -664.5	-664,5	-277.4	-488.1	-783.6	-462.0
$log(TMD+10) = b_{1}-19 C_{1-19} + b_{23} (T_{V/L}=20^{-}120.3)$	2.7	1.8	1.8	1.4	2.5	2.2	2.2	2.1	1.7	1.9
$log(TMD+10) = b_{1-19} C_{1-19} + b_{24} (X158-33.7)$	2.7	1.8	2.8	1.4	2.5	2.2	2.2	2.1	1.8	1.9
log(TWD+10) = b ₁₋₁ 9 C ₁₋₁₉ + b ₂₅ (RVP-12.4)	2.7	1.8	2.8	1.4	2.5	2.2	2.2	2.1	1.7	1.9

NOTE: Underlined coefficients are not significant at 95% confidence.

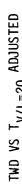
TABLE F.11 (Continued)

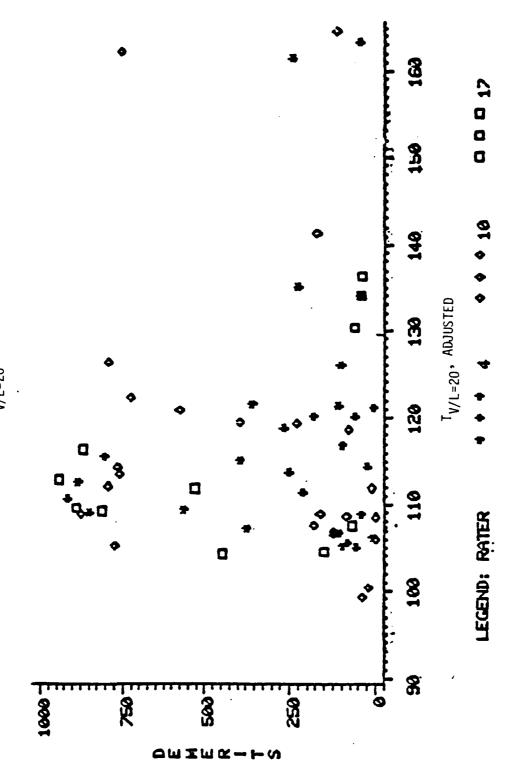
REGRESSION EQUATIONS - TWO AS A FUNCTION OF FUEL PROPERTIES

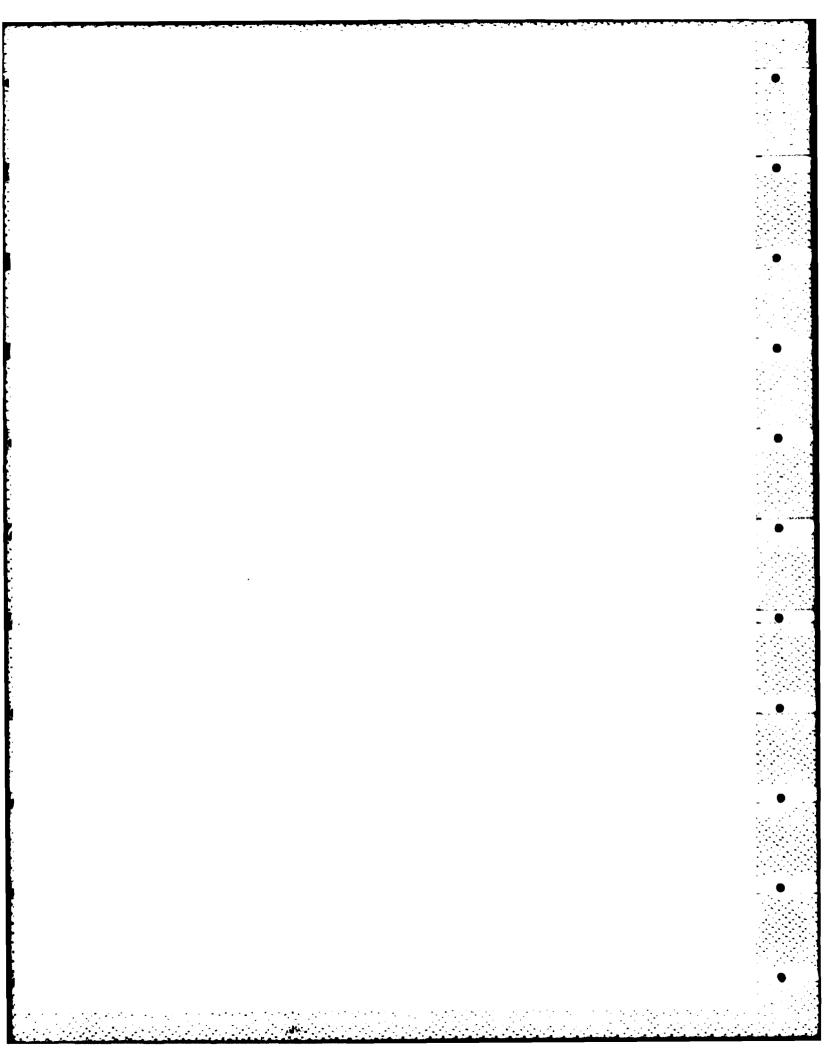
		æ	Regression Coefficient	Coefficie	į			
Equation Form	-02 0 -	-12 -	<u>-</u> 20- <u>-</u> 21- <u>-</u> 22- <u>-</u> 223- <u>-</u> 224- <u>-</u> 225-	<u>-6</u> 23.	<u>-</u> b 24-	<u>-625</u> -	r 2	RMS
IMD = b ₀ + b ₁₋₁₉ C ₁₋₁₉ + B ₂₀₋₂₂ R + b ₂₃ T _{V/L=20} + b ₂₄ *158 + b ₂₅ RVP	206.6	0.0	- 59.5	-20.4	4.7	-81.7	0.75	200.2
$log(1MD+10) = b_{1-19} C_{1-19} + b_{23} (V/L=20-120.3)$	1	;	1	-0.1	;	ł	0.79	0.30
$log(1MD+10) = b_{1-19} C_{1-19} + b_{24} (x158-33.7)$:	!	:	;	0.12	1	0.78	0.31
log(TWD+10) = b ₁₋₁₉ C ₁₋₁₉ + b ₂₅ (RVP-12.4)	1	;	;	;	;	90.0	0.79	0.30

NOIE: Underlined coefficients are not significant at 95% confidence.









APPENDIX G

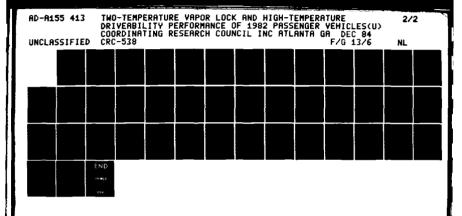
1982 CRC VAPOR LOCK TEST DATA

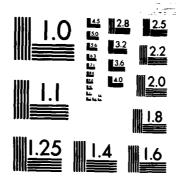
		•	1702 (שאל שאל	-date	ahr	,	. K g 710					
Car#:	7 1					_			ata (Commer	nts: N	0	
				euibf Adjust				•					
Run#	Date	Drvr	Obsr	DATA- Fuel	AirT	Wind	RVP	T2Ø	T2ØA	Accel -50	lerati -6Ø		Surg
1	921	1	5	9	106		1183	1226	1149				т
2	922	i	5		109		1242				188		•
3	922	ī		5			943				191		
4	922	1	5		1Ø8		697				192		
5			5	1	93						197		
6		ī	5	÷	98						178		
	/=-	•		_	, •		g	ø	ø				
							ēs	ø					
							•			124.	185.	354.	
			CEY-OF	FF SOA	K COM	NDITIC	NS		<u>-</u>		~		
Run#									Sky	Wind	Star	ting	
		Air	TcA	TcB	Air	TcA	TCB	AirT			sec	RSt#	
-1	49Ø	106	139	110	105	150	110	1Ø55	SN		2		
								Ø					
								Ø					
								Ø		,			
								Ø					
								Ø					
								Ø					
				FF SO									
				-6Ø					T2Ø	T2ØA			
				%Inc									
1	132	7	194		378			118/	1224				
		Ø		Ø		Ø			(2)	Q G			
		Ø		Ø		Ø			Ø	Ø			
		Ø		ଡ଼		Ø			Ø	હો હો			
		Ø		Ø		Ø Ø			Ø Ø				
		ୟ ହ	-	ହ ହ		Ø			Ø				
			TDIE (30AK (וזמאחר								
Run#										We ad	Star	tina	
		Air		TcB			TCB					_	
1	474	105		113	1Ø5		112						
2		109			109			1090			2		
3	475	109	161	120	109			1090	SN		3		
4	457	108	142	123	108	_	122		SN		2		
5	59	93	129	106	93	174	•	-930	SN		_		
6	88	98	135	114	99		110		SN		3		
		_	-					Ø					
				SOAK A									
Run#	15-	-5Ø	15-	-6Ø	15-	-7Ø	Surg	RVP.	T2Ø	T2ØA			
	Time	%Inc	Time	%Inc	Time	%Inc							
1	175	42	278	5Ø	559	58		1Ø98					
2	161	3Ø	25Ø	35	499	41		1197					
3	146	18	238	28	527	49		997					
4	146	18	229		481		M						
5	132	7		11	449				1465				
6	161	<i>30</i> 1	270	46	510		Н	1160					
		Ø		Ø		Ø			Ø	Ø			

			1702 (LAC K	egurar	vabo)r L0(CK, FC	J.				
Car#:	Ø2		Temp_			=. 7@F	=/1.ØF			Commei	nts: 1	₹ԱՌ 1	
Run#	Date					Wind	RVP	T2Ø	T2ØA				-
1	1004	17	7	14	95		1475	1086	10004				
	1004	17	7	17	94			1020					
		17	7	1	89			1532					
•	12.2.0	1	•	•	· ·		Ø	g	Ø	4 44	,_	722	
							ø	ģ					
							Ø		ø				
							ø	gi gi					
							gi gi	gi gi					
							K,	y,		1 70	222	707	
			<ey-of< td=""><td>F 50</td><td>ak con</td><td>DITIO</td><td>DNS</td><td></td><td>_</td><td>138</td><td></td><td></td><td></td></ey-of<>	F 50	ak con	DITIO	DNS		_	138			
Run#	Smp#							Avg				rting	
		Air	TcA	TcB	Air	TcA	TcB	AirT			sec	RSt#	
1	200	95			94			945				1	
2	182	94			92			930			3	1	
3	234	9Ø			9Ø			9ØØ	SN		1		
								Ø					
								Ø					
								Ø					
								Ø					
								3					
								RVP					
								·					
			164					1514					
2			17Ø	-27	23Ø	-41		1627	1026	18148			
3	112		176	-24	3Ø4			1241	1196	1231			
		Ø		Ø		Q			Ø				
		Ø		Ø		Ø			Ø	21			
		Q1	-	Ø		Ø			ଡ଼	21			
		Ø		Ø)		Ø			Ø	Ø			
								Avg				ting	
		-	ICA			ICH	102	AirT			sec	RSt#	
	159	94		-	93			935	SC				
	198	92			91			915	SC				
3	243	90			91			905	SN				
								Ø					
								Ø					
								Ø					
			IDLE S	במעה י	יררבו ה	PATT	NC	ହ					
P #								RVP	TOG	T2ØA			
			Time				_	17 A L	1 4 X'	7 4 X/FI			
1	108	-22	164	-30	262	-32		1441	1101	1111			
2	106	-23	168	-28	256	-34			1063				
3	110	-20	174	-25	298	-23			1204				
•	~	Ø	- ′ ′	Ø		Ø		'	Ø	g			
		ø		Ø		Ø.			Ø	Ø			
		ĢI		ø		Ø			ŽI	ģī		1	
		Ø		Ø		ø			ø	ģ		1	
						-						;	

		-									•		
Car#:	3					=.7ØF	CRC Fu F/1.ØF	=		Commer	nts:	No	
Run#		Drvr	Obsr	Fuel	AirT	Wind	RVP	TZØ	T2ØA	Accel -5Ø		i ons- -7Ø	
1 2 3 4	921 922	12 12 12 12	16 16 16	9 14 16 17	1Ø6 99 1Ø9		1183 1475 1588	1226 1Ø86 1Ø41 1Ø2Ø Ø	1149 1Ø58 943. 922. Ø	1Ø8 116 1Ø8 11Ø	149 151 154	199 194 212	т
							Ø Ø	Ø Ø	Ø	111.	151.	2Ø2.	
		 	CEY-OF	F SOA	AK COM	VDITIE	JNS						
1	494	Air 106	TcA 147	T⊂B 12Ø-	Air 105	TcA 17Ø	TcB 1Ø8 1Ø3	AirT 1Ø55	SNP		Star sec 1Ø 2	RSt#	
2	436	77	142	.114	166	170	120	9 9 9 9	21414				
			(EY-OF	F SO	AK AC	CELERA	PLONE	3					
Run#	15-	-5Ø	15-	-60	15-	-7Ø	Surg	RVP	T2Ø	T2ØA			
	Time												
	11Ø												
2	124	12	160	6	2Ø7			1366	1134	1103			
		ଥ		Ø		Ø			Ø				
		Ø		Ø		Ø			Ø				
		Ø T		Ø		Ø			Ø				
		Ø		Ø		Ø			Ø Ø	ୟ ସ			
		Ø		Ø SOAK (Ø CTONG:							
Pun#							ad					ction	
							TcB					RSt#	
1	497	1Ø5					120						
2	499	1Ø1	147	118	102	174		1Ø15	SNN				
3	482	197	148				115		SNN				
4	47Ø	109					113	ญ ช Ø	SNN				
							DNS						-
							Surg		120	T2ØA			
	113	%1nc 2	11 me 156_			%1nc		1092	1274	1204			
1 2	121	10	170		225	11	T						
3	120	9	170	13	221	9	Ť	1303	1164	1063			
4	118	7	17Ø	13	225		•		1140				
		Q1		Ø		Ø			Ø	ହ			
		Ø		Ø		Ø			ହ	Ø			
		Q1		Ø		Ø			Ø	ହ			

					edare.	vap	O,	CK, M	Οť			
Car#:	Ø4									C	nts: No	
			Temp (Ad ius	tment	= 701	E/1 0	E GEI D	ata	Cowwei	nts: No	
			BASE	DATA				' 				
Run#	Date	Drvr	Obsr	Fuel	AirT	Wind	RVP	T20	TOGA	Acce	lerations	- Sura
								~~~~		-50	-60 -70	_
1	1006	17	7		93					138		
	1012		7	15	85		1532	1062	1132	132	218 333	
3	1013	17	7	17	85		1644	1070	1000	177	₹40	
4	1013	17	7	15	87 9ø		1532	1Ø62	1118	136	218 364	
5	1013	17	7	13	9Ø		1417	1111	1146	132	214 326	
							Ø	Ø				
							Ø	Ø	Ø			
							Ø	Ø Ø	Ø			
									Avq:	134	217 346.	
		k	EY-OF	F_S0	ak con	ודומי	NS					
Kun#	Smp#	-Tmp	a_Sta	art	Tmp	) a Er	nd	Avg	Sky	Wind	Starting	!
		Alr	TCA	TCB	Air	TcA	TcB	AirT			sec RSt#	•
1	244	93	127	118	92 85 86 89	151	138	925	SN		2	
2	286	85	120	109	85	144	116	85Ø	SN		1	
<u>ن</u> م	324	85	116	108	86	145	125	855	SN		3	
4	346 	88	118	110	89	. 45	132	885			2	
5	نانان	90	120	112	89	151	129		SN		2	
								Ø				
							~	ଯ				
Run#	15_	 	<u> </u>	r SUF	AK ACC	ELERA	TIONS	5				
	Time	7 toc	T: 55	***	15- Time	·/ <u>//</u>	Surg	RVP	T2Ø	TZØA		
1	146	/• ± 1 1 C	224	711C	740	%1UC		1711	4.55			
2	148	101	257	15	362 414	ე ეფ		1514	1159~	-1-1-77		
3	258	93	570	140	790	120		131/	1608	1138		
4		6	<del>200</del>	スマロ	496	140	. п м	1/61	10000	1967		
5		1 &	262	21	424	23	11	1334	1000	1699		
		Ø		Ø	727			1707				
		Q)		ହ		ดี		~	Ø	ର ଧ		
		I	DLE S	OAK C	CNDIT	ICNS-						
Run#	Smp#	-Tmp	9 Sta	rt	Tmp	a En	d	Ava	Skv	Wind	Starting	
		Air	TcA	TcB	Air	TCA	TcB	AirT			sec RSt#	
1	225 .	- 91	126	121	90	155	136	9Ø5-	SN		522 7.50.	
2	292	85	116	107	85	127	118	85Ø	SN			
3	319	87	118	$1.1  \mathrm{x}^{\mathrm{s}}$	87	151	131	87Ø	SN			
								Ø				
								Ø				
								Ø				
		<b>.</b>					_	Ø				
D.,_#		[]	DLE S	DAK A	CCELE	RATIO	NS					
Run#	10-:		15-6	5Ø	15-1 	7ダーー !	Surg	RVP	TZØ	T2ØA		
					Time :							
2	142 134	6	25ø	15	378	9		1283				
3	148	Ø 10	216	্ব	342	-1		1475				
J	170	10 0	252	16	67Ø	93	T	1576				
		QT		<i>ପ</i>		Ø			Ø	(3)		
		y. Ø		Ø Ø		ହା ଫ			Ø	Q1		
		Ø Øl		Ø		Ø			Ø	Ø		
		×,		£1		Ø			Ø	ÇI		





MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS-1963-A

						·							
Car#:	Ø <b>5</b>	•	Temp /	adjust	tment	=. 7ØF	F/1.Ø	<b>F</b>			nts: N	40	
		Drvr	Obsr	Fuel		Wind	RVP	T2Ø	T2ØA	Acce	lerati -40	ons-	_
	1005	17								166		328	
	1996	17			91					124		294	M
	1004	17	<b>,</b>	•	07		407	1572	1514	114	100	277	11
3	1000	1/	<b>'</b>		73		1004	1302	1340	110	102	208	
=	1012	0		0	B/		1994	1228	1084	110	178	264	
5	1812	8		8	87		1124	1258	1300	111	182 178 176 178	246	
•	1012	8	2	4	88		882	1405	1454	115	178	260	
							Ø	Ø	Ø				
							Ø	ø					
											179.	257	
					ak cov							<del></del>	
											Star		
		Air	TCA	TCB	Air	TCA	TCB	Airt			580	RSt#	
1	189	91	152		71	196		910	SN		2	1	
2	232	91	151		92	192		915	SN		2	2	
								Ø					
								Ø					
								Ø					
								Ø					
						· <b>x</b>		Ø					
					AK ACC 15-								
	Time	%Inc	Time	%Inc	Time	ZInc							
	152				3Ø8							·	
		5	182	-2	254	-1	M	1254	1188	デブデフ			
_		ø		<u></u>	254	ā	••		a	a			
		Ø		ø		ø			ø	ø			
		Ø		ø		ø			ø	ø			
		Ø		ø		ø			õ	ø			
		Ø		ø		∡ Ø			ø	ø			
		<u></u> ]	DLE S	OAK C	CONDIT								
Run#	Smp#		a Sta	rt	Tmp	9 En	d	Ava	Skv	Wind	Star	tina	
:		Air	TCA	TcB	Air	TcA	TcB	AirT			sec :	RSt#	
1			148		91	177		910	SN	-		· · • • • • • • • • • • • • • • • • • •	
2					- 92	200		92Ø					
3	226	93	152		93	196		930	SN				
4	343	87	155	88	87	198	97	87Ø	SN				
5	332	89	151	99	9ø	196	98	895	SN			1	
6	325	88	154	99	87	195	95	875	SN			•	
_			- <b>-</b> .	• •	<del></del>	- · <del>-</del>	•	Ø					
		1	DLE S	IDAK A	CCELE	RATIO	NS						
Run#	15-	5ø	15-	60	15-	70	Sura	RVP	T2Ø	T2ØA			
					Time							•	
1	174	52	232		. 310	21			1149	1177			
2	190	66	254	42	332	29			1204		•		
3	170	49	238	33	31Ø	21			1191				
4	137	2ø	206	15	290	13			1278				
5	148	3ø	210	18	285	11			1218				
6	117	2	181	1	269	5	• • • • • • • • • • • • • • • • • • • •		1342				
_		ā		ġ		Ø		701	1342 Ø	1373			
		_		~		×.			X.	v			
	_		_										

Car#:					tment	=.7ØF	=/1.ØF	•			nts: F		
Run#	Date	Drvr	Obsr	Fuel	AirT	Wind	RVP	T2Ø	T2ØA	Acce: -50	lerati -60	ons- -70	Surg
													T
• 1	. — -	1	5		106						178 176		J
2		1	2	12	1Ø5								н
3		1	2	16	95						172		л
4	922	1	5	1	100 110						158		
5	922	_ 1	5	17	110				_	144	199	276	Н
							Ø	Ø	Ø				
							Ø	g.			`		
							Ø	Ø					
									Avg:				
											Star		
			TCA								sec	RSt#	
	496				106	193	111	1060	5N		5		
	473	105	149	118	105	190	108	1050	SN		3		
	495				97						3		
4	454	100	146	117	102	183	112		. SN		2		
								Ø					
					•			Ø					
								Ø					
					AK ACC								
					15-								
		%Inc	Time	%Inc	Time	%Inc							
	116				252								
	116				241								
3	119	11	181	15	257	15	Н	1439	1101	1094			
4	116	8	1.73	- 9	237	6	. H	1100	1272	1230			
		Ø		Ø		Ø			Ø	Q			
		Ø		Ø		Ø			Q	Ø			
		Ø		Ø		Ø				Ø			
					CONDIT								
											Star		
			TcA	TcB	Air	TcA	TcB	AirT			sec	RSt#	
		106			1Ø6								
2		105			105				SN	•		•	
					99								
	479			116			116		SN				
5	462	1Ø7	153	106	108	182	106	1Ø75	SN				
								Ø					
								Ø					
					ACCELE								
					15-					T2ØA	•		
					Time								
1	125	17		22	272	21			1292				
2		10	180		252				1260				
3		8							1160				
• 4		11	176	11	252		Т						
5	129	21	216	37	350	. 56	Н	1371	1132	1045	•		
		QI		Q		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			

		_			- 4 ~ - ~ .								
Car#:	7					· · · · ·	RC F	mal Da	ta (	Commer	nts: F	iuns :	₹. 5
	•	•	Temo é	ad just	tment					J-0,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			-, -
Run#	Date	Drvr	Obsr	Fuel	AirT	Wind	RVP	T2Ø	T2ØA	Accel	lerati	ons-	Sura
										-50	-6Ø		
1	921	12			106					158		348	М
2	922	12			97								M
3	922	12	16	1	103					142			- *
4		12	16	16	108		1588	1041	95ø.	210			н
		12	16	14	111		1475	1086	974.				
6	922 923	17	16	13	111 99		1417	1111	1083	158	230		
7	923	17	16	14	1Ø3		1475	1086	1030	180	251		
•	,	• •		• •			g	ø	Ø				• •
							•	_		142	21Ø	3Ø1	
			KEY-OF	FF SO	AK CON	DITIC	INS						
											Star	tina	
			TcA	TcR	Air	TEA	TcB	AirT			sec	RSt#	
	486	196			- 106						1		
2		97			99						ī		
3	459				105						2		
4		1Ø8			107						3		
5	30	111			111						4	1	•
6	95				100						3	1	
7	21				105						3	-	
					AK ACC						•		
					15-								
					Time								•
					322								
2	130	-8	195	<b>-7</b>	289	<u>-4</u>	• ••	1057	1297	1276			
3	1 44	1	212	1	289 3Ø7 474 377	2	т	777	1476	1413			
4	225	58	330	57	474	57	н	1404	1117	1029			
5	193	34	258	23	377	25	M	1299	1166	1054			
6	159	12	232	10	329	-9	н.	1342	1146	1114			
			251	20	368		H						
			IDLE S	SOAK (	CONDIT								
											Star	tina	
											580		
	498				106								
			134	112	99	172	111	990	SNN				
3	163	106	142	118	107	174		1065	SNN				
4	471	108		112	108	169	_	1Ø8Ø	SNN				
5	19	111	142	114	110	175		11Ø5	SNN				
6	97	1Ø1	138	111	101	162		1010	SN				
=					• • •		•	ø					
			IDLE S	SOAK 4	ACCELE	RATIO	)NS						
					15-					T2ØA			
					Time								
1	141	-1	212	1	300	ø		1072	1288	1211			
2	161_		225	7	318	6		1024					
3	156	10	221	5	320	6		768					
4	190	34	260	24		21		1240					
5	2Ø8	46		37	410	36		1153					
6	155	9	238	13	343	14		1247					
_		ø		ø		Ø		• •	Ø	Ø			
									_				

		•											
Car#:	Ø8							_	ata (	Commen	ts: N	lo	
		•	Temp /	Pd just	tment	=.7ØF	-/1.ØF	=					
Run#	Date	Drvr	Obsr	Fuel	AirT	Wind	RVP	T2Ø	TZØA	Accel		ons-	Surg
										-5Ø	-60	-7Ø	
1	922	4	10	15	1Ø3		1532	1Ø62	1006	91	137	2Ø2	
2	922	4	1Ø	17	1Ø8		1644	1Ø2Ø	929.	94	139	2Ø8	
							Ø	Ø	Ø				
							Ø	Ø	Ø				
							Ø	Ø	Ø				
							Ø	Ø	Ø			•	
							Ø	Ø	Ø				
							Ø	Ø	Ø				
							_	_		92.5	138	2Ø5	
			KEY-NI	F SO	AK CON	DITIC	INS						
										Wind	Star	ting	
		103	167		105	,			SN		2		
2	469	108			108			1000	SN			· 1	
~	407	TKO			1 2/0				214		,		
								Ø					
								Ø					
								Ø					
								. Ø					
								Ø					
					AK ACC						•		
					15-								
					Time								
	, 91				2Ø3								
2	92	-1	136	-1	2Ø4	Ø		1363	1136	1045			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Q1		Ø		Q)			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
			IDLE S	SOAK (	TIGNO	IONS-							
Run#:										Wind	Star	ting	
					- Air							RSt#	
1	483	196			107			1965	SN				
2	487	1Ø9			110			1Ø95	SN				
								Ø1					
								Ø					
								Ø					
								ø					
								ø					
			IDLE 9	BOAK 4	ACCELE	RATIC	NS	-					
Run#					15-				T2Ø	T2ØA			
					Time								
1	92	-1	134	-3	201	-2		1190	1222	1142			
2	95	3	141	2	220	7			1234				
4	73	gi		ā		ø		1107	1234 Ø	113 <u>2</u>			
		Ø		Ø		Ø			ø	ø			
				Ø		Ø			ø	Ø			
		Ø											
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			

		-	1982 (	JRU RE	egu i ar	- vapo	or Loc	:K, MC	) C				
Car#:	σο	•					EC E	el Da	 a+-a f	Commer	nts: N	lo.	
Cel H.	x, ,	-	Temp 4	ad inet	ment	=.7ØF					,	•	
						-							
Run#										Accel	lerati	ons-	Sura
1	922	4	10	4	112		882	14Ø5	1286	152	23Ø	374	
2	923	17			105		1064	1293	1223	140	21Ø	360	
3		17			106			1226					
4		17			93			1111					
5		17						1165					
6		17						1226				342	
7		•		•			Ø	Ø	Ø				
•							Ø	ø					
							•-			143.	213.	356	
			<ey-of< th=""><th>FF SDA</th><th>ak con</th><th>NDITIO</th><th>NS</th><th></th><th></th><th></th><th></th><th></th><th></th></ey-of<>	FF SDA	ak con	NDITIO	NS						
Run#										Wind	Star	tina	
	•	-							-		sec	_	
1		112						1115					
2				125		156	144				4		
3						155					4		
· <del>-</del> '	~ <b>.</b>	150	101	120	12.0	100	170	Ø	214		7		
								ø					
								ø					
								ā					
			/EV_06	en/	אי ארנ	CELERA	אד ז האופ	-					
						-7Ø							
						%Inc							
	150	5	230	Ä	398	6 12	т	1072	1288	1218			
	152	<u> </u>	249	17	398	12	M	1156	1241	1164			
•		ø	7 /	Q)		ø		1100	Ø				
		ø		ā		ø			ø				
		ø		Ø		Ø			ø				
		ø		Ø		Ø			Ø	-			
			IDLE 9		CONDI	TIONS-							
Run#											Star	tina	
						TcA						RSt#	
1				,		,		1110				,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
			147	125		169			SN				
3	1		133		107				SN				
4	43	93			93			930					
Ś	85	94		116				940					
5	76	191				169		1010					
-	, •	4 /4' 4		1.10	***	10,	• • •	Ø					
			IDLE S	SOAK 4	ACCEL	ERATIO	NS	-					
						-7Ø				T2ØA			
						%Inc							
1	_	15		15	4Ø5	14		868		1302			
2	154	8		7	382	7		1036	1309	1236			
3		5	275	29	415	17	Н	1105	1269	1185			
4				84		57							
5		12		93		55							
6		6				17							
_	<b>-</b>	ø		ø		Ø			<u>@</u> l				
									-	-			

_		•								_			
Car#:			r /	المستقامة	tment			_			nts: N		
			BASE	DATA-		/ Łif	- / 1 . E/F						-~
Run#	Date	Drvr	Obsr	Fuel	AirT	Wind	RVP	T2Ø	T2ØA	Acce:	lerati	ons-	Surg
	924	17									160		
	924		16	4	1Ø1		882	1405	1363	114	167	245	
3	924	17	16	1	104		697	1532	1469	112	163	237	*
4	1004	2	8	2	94		/57	1488	1475	93	129	185	T T
5	1004	2	8	1	93		67/	1002	1046	75	129 133 146	219	•
٥	1914	1/	,	2	41		021	1445	14/3	70	146	ZZK	
										115	163.	245	
							7	ava 4.	5.6=	95.3	136	205	
		i	CEY-OF	F 504	ak con	ודומע							
											Star		
											sec		
					99								
		_	-					Ø					
								Ø					
4	17Ø	95	120	118	95	140	116	95Ø	SC	•	3		
								Ø					
								Ø					
		,						ø					
					AK ACC								
					15- Time								
	115				363								
•	113	Ø	200		200	ø		A A 77	Ø				
		ø		a		Ø			ø	20			
4	1Ø9		155	14	236			1206					
•		Ø		Ø		ø	•			Ø		-	
		ø		Ø		Ø			Ø				
		Ø		Ø		Ø			Ø	Ø			
	****		IDLE S	SOAK (	CONDIT	riens-							
	Smp#	-Tmp	a sta	art	Tmp	a_Er	1d	Avg	Sky	Wind	Star	ting	
											sec	RSt#	
					100								
-					101				CL				
3 4	29	104	143	133		169	_	1045	CL SC				
4 5	154 186	94 93	12Ø 118	121 118	94 92	145 147	140	94Ø 925	SC				
6	315	73 91	122	124	91	148	139		SN				
	313	7.	122	127	7.	170	107	Ø	511				•
			IDLE S	BOAK A	CCELE	RATIO	)NS						
Run#					15-					T2ØA			
	Time	%Inc	Time	%Inc	Time	%Inc							
1	132	14	478	193	518	112		1148					
2	162	40	512	213	72Ø	194		1Ø88					
3	122	6	2Ø3	24	357	46		881					
4	103	8	151	11	264	29		1181					
5	96	1	144	6	246	2Ø	M	1248					
6	104	9	148	9	222	8		884	1404				
		Ø		Ø		Ø			. 0	Ø			
									_			•	

		-											
Car#;	11		•			(	CRC F	uel Da	ata (	Commer	its: F	Run 1	
		-	Temo /	Ad iusi									
			DACE	DATA.									
D.,	Data	Desar		End;	AirT	144	DUD	T20	TOGA	Accel	arati		Suca
nun#	Dace	DEVE	UUSI	LUEI	M17 1	MILIO	LAF	120	1224				
										_			~
1	924	17			1Ø2							4Ø9	
2	924	17	16	1	106		697	1532	1455	162	256	357	
3	1004	17	7	3	92		821	1445	1466	142	216	310	
	1004		7	5	90		943	-1366	1401	138	210	300	
	1005		7		91		1124	1258	1284	144	224	330	
	1006	17	ź	10	00		1242	1105	1277	170	214	306	
			<u> </u>	16	92 90 91 89 92 87		1274	1170	123/	170	210		
	1006	17			92		1004	1273	1314	120	214	3Ø4	
	1Ø12	17	7	7	87		1064	1293	1349	140	216	3Ø4	
	1Ø12			10	84		1242	1170	12/2	142	228	330	
1Ø	1Ø13	17	7	_ 3	87		821	1445	1501	142	216	. 310	
	1Ø13		7	.13	9Ø		1417	1111	1146	142	222	312	
12	1013	17	7	15	89					140		312	
		• •	•		٠,					141.		312.	
			/EV_06		AV CON		3NIC						
					ak CON								
					Tmp								
		Air	TCA		Air							RSt#	
1	68	102		139	103		154	1 <i>Ø</i> 25	CL		2		
2	- 36	106		14Ø	107		152	1065	CL		1		
3	177	92	123	. 122	93	192	143	925	SC		1		
4	213			122	93 89	194	139	895	SC		2		
5	236	91	150		91		139				ī		
		90	(30		91		147				2		
6	231												
7	224		138		93		149				1		
8	273	87	124	114	86	194	133	865	SN		1		
- 9	312	84	- 114	12Ø	84 87 89	179	126	84Ø	SN		1		
10	322	87	116	119	87	194	134	87Ø	SN		2		
11	318	89	118	120	. 89	193	145	89Ø	SN		2		
12	323	. 89	124	119	88	193	143	- 885.	SN		2		
			CEY-OF	F 504	AK ACC	ELER4	TIONS	3			_		
					15-						•		
	T:	***	7:	* T = -	Time	7 T	our g	.7177					
		71nc	11me	41nc	111111	71NC		1.605	1000	<b>-</b>			
	174	24	28/	32	423 537 37Ø	36		TNAAA	12/7	1220		•	•
2	172	22	31Ø	42	537	72		774	1478	1397			
3	152	8	236	8	37Ø	- 19		1228	1202	122Ø			
4	134	-5-	216	1	332	6		1260	1186	1224			•
5	152	8	_	2Ø	434	39				1217			
6	160	14		2Ø	414	33				1189			
7	154	9		16	396	27				1196			
-	142			8						1312			
8		1	236										
9	148	5	238	9	402	29				1234			
1Ø	148	5	228	5		9				1456			
11	152	8	234	7		16				1133			
12	158	12	24Ø	10	358	15		1611	1Ø32	1977			

CRC Fuel Data Comments: Run 1 Car#: 11 Temp Adjustment = .70F/1.0F - BASE DATA----Run# Date Drvr Obsr Fuel AirT Wind RVP T20 T20A Accelerations- Surg -50 -60 -70 ..... -----924 17 16 9 1Ø2 1183 1226 1177 174 276 4Ø9 <del>-</del> 1 924 17 1 106 697 1532 1455 162 256 357 2 16 3 1004 17 7 3 **92** 821 1445 1466 142 216 310 7 5 90 17 943 1366 14Ø1 138 210 300 4 1004 7 8 5 1005 17 91 1124 1258 1286 146 224 330 6 1006 17 7 10 89 1242 1195 1237 138 216 306 7 1006 17 8 1012 17 7 7 92 7 7 87 1064 1293 1314 138 214 304 1064 1293 1349 14Ø 216 **3Ø4** 10 1242 1195 1272 228 9 1012 17 7 84 142 33Ø 7 10 1013 17 .3 87 821 1445 15Ø1 142_216_310 13 1417 1111 1146 142 222 312 11 1013 17 7 9Ø -15 1532 1062 1104 140 218 312 12 1013 17 89 Avg: 141. 218 312. ---IDLE SOAK CONDITIONS Run# Smp# -Tmp @ Start-- -- Tmp @ End--- Avg Sky Wind Starting --- --- Air TcA TcB Air TcA TcB AirT --- --- sec RSt# 140 143 104 173 1040 9Ø 1Ø4 _ 87 1Ø7 137 107 175 1Ø7Ø CL -----IDLE SOAK ACCELERATIONS-----Run# --15-50-- --15-60-- --15-70-- Surg ,RVP TZØ TZØA --- Time %Inc Time %Inc Time %Inc ---- ---- ---

998 1332 1269

762 1486 1402

NOTES: Runs included in base acceleration time averages: 3-10 RVP is psix100; T020V/L & Avg Air Temp are deg Fx10; Acceleration times are sec.x10

434

Ø

39

Ø

39

1

198

· Ø ·

3Ø3

41

		•	1702 (	-UC VE	ryus ar			- N 9 110					
Car#:	12						CRC FL	uel Da	ata (	Commer	nts: !	٧o	
				teui bf -ATAD				<del>-</del>					
Run#				Fuel	AirT	Wind	RVP		T2ØA				
										-5Ø			
1	922	1	5		112					1Ø9			
2	923	1	5	9	95					1Ø4			
3	923	1	5	5	97		943	1366	1352	1Ø1	149	2Ø4	
4	923	1	5	7 · 8	99		1Ø64	1293	1265	97	142	197	
5	923	1	5	. 8	1Ø4		1124	1258	1195	109	163	219	
							Ø	Ø	Ø				
							Ø	Q1	Ø				
							Ø	Ø	Ø				
							-	_		1Ø4	154.	210.	
÷			KEY-O	FF SOA	AK COM	DITION	)NS		_				
Run#	Smp#	-Tmp	a Sta	art	Tmg	o a Er	nd	-Avg	_Sky	Wind	Star	rt <u>i</u> ng	
	<u>`</u>	Air	TcA	TCB	Air	TcA	TcB	AirT			sec	RSt#	
1				13Ø							9		
-	- '					•••		Ø		•	•		
								ø					
								ø					
								Ø					
								Ø					
								2) 21					
		1	/EV_0I	FF SOA	N ACI	-C)	AT T ONE	-					
		-		-6Ø									
				%Inc						1227			
	1 T WG									1170			
1		108			٠.,	223		1202					
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø				
		Ø		Ø		Ø			Ø	ହ			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
				SUAK (									
				art									
				TcB							sec	RSt#	
1	4	111		132									
2	92	95	136		95	174	151	95Ø	SN				
3	28	97	140	129		174	148	97Ø	SN				
4	93	99	143		100	169	148	995	SN				
5	98	1Ø5	142	131	1Ø5	178	151	1050	SN				
								Ø					
								Ø		-			
				SOAK A									
				-6Ø			_		T2Ø	T2ØA			
				%Inc					4===	4665			
1	115	11		97	423	101		965					
2	112	8	231	5ø	327	56	н	1164					
3	107	3	158	2	219	4			1327				
4	106	2	153	-1	242			1071					
5	1Ø9	5	162	5	316	5Ø	Н	1069	129Ø				
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			

			1702 (	K	egus ar	vapt	Jr LOC	- N 9 FIL					
Car#:	13						CRC F	el Da	ata (	Commer	1+== -l	40	
Cal W.	10	•	Temp A	ad inet	tment				, ,			••	
	· 		BASE	_									
Run#			Obsr								erati	ions-	Sura
										-50		-7Ø	
1	922	1	5	9	111		1183	1226	1114	89	131	172	
2	923	1	5				1183	1226	1219	84	125	182	
3			5				1417	1111	1090	<del>9</del> 7	139	.93	
4			5							98			T
5	923	1	5	17	1Ø5					93			
_			_				Ø		Ø				
							Ø	Ø	Ø				
							Ø	Ø	Ø				
	_								Avg:	92.2	134.	186.	
			KEY-OF	FF SOA	AK CON	VDITIO	)NS						
	Smp#	-Tmp	a Sta	art	Tmc	a Er	nd	Ava	Sky	Wind	Star	ting	
		Air	TcA	TcB	Air	TcA	TcB"	AirT			sec	RSt#	•
. 1	44	111	147		110	160		11Ø5	SN		2		
								Ø					
								Ø					
								Ø					
								Ø					
								Ø					
								Ø					
			CEY-OF	F SOA	AK ACC	ELERA	ATIONS	3					
Run#	~~15-	-5ø	15-	-6Ø	15-	-7Ø	Surg	RVP	T2Ø	T2ØA			
			Time										
	97				196								
		Ø		Ø					Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
			IDLE S										
Run#	Smp#		9 St.							Wind	Star	rting	
		Air	TCA	TcB	Air	TcA	TcB	AirT			sec	RSt#	
1	5	110	138		110			1100	SN				
2	<b>99</b> .	97			97	15Ø		97Ø	SN				
3	37	99	13Ø		99	150		990	SN				
4	₹		13Ø		1Ø1	152		1010	SN				
5	23	1Ø5	134		1Ø5	152		1050	SN				
								Ø					
								Ø	_				
			IDLE S										
			15-					RVP	T2Ø	T2ØA			
			Time										
1	110	19	161	2Ø	225	21	Т		1332				
2	100	8	145	8	203	9			1225				
3	112	21	167	25	227		_		1171				
4	111	2Ø	160	20	224		T			1093			
5	114	24	167	25	226	21		1327	1153				
	•	Ø		Ø		Ø			Ø				
		Ø		Ø		Ø			Ø	. Ø			

		•	1782 (	SAC RE	zānī ai		Jr 600	- N g   FIL	J C				
C	1.4	•					PP E		- <del>-</del>		nts: N	do.	
Car#:	14		T /	٠					aca (	Jonnei	ICP: I	<b>10</b>	
					tment								
Ruo#					AirT						erati	005-	Sura
1	922				110			1226					
2	923			7	78		1100	1744	1745	04	138	224	
3	923	17 17		7	1Ø1		1014	1207	1251	727	130	223	
3 4		17	10	<b>,</b>	105		1107	1273	1154	97	130		
												227	
5			. 10	0	106		1124	1226	1244	70 05			
6		17		7	93	•	1100	1220	1207	73	139	208	
/	1014	1/	/	8	90			1258		84	132	224	
							Kı	Ø		A 7		207	
							3510				134.	223.	
					ak con						~~~~		
Run#					Tmp								
					Air							RSt#	
1	33	110	162	130	110	216	172		SN		3		
								Ø					
								Ø					
								Ø					
								Ø					
								Ø					
		_						_ Ø					
					AK AC								
Run#	15-	-5Ø	15	-60	15-	-7Ø	Surg	RVP	T2Ø	TZØA			
		%Inc	Time	%Inc	Time	%Inc							
1	87		215	_	300			1148					
		Ø		6		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	ø			
		Ø		Ø		Ø		-	Ø	Ø			
					CONDIT								
	-				Tmp								
_					Āir						sec	RSt#	
ŀ	45	110			110				SN			•	
2	28	98	138		99		15ø	985	SN				
3	94	101	140		101	173		1010	SN				
4	46	1Ø5			105	193		1050	SN				
5	10	106	135		197	188		1065	SN				
6	6	93	131	113	93	183		930	SN				
7	380	90	125		9Ø	167	143		SN				
					ACCELE								
					15-				T2Ø	T2ØA			
					Time								
1	9Ø	-2			371	67		1058					
2	94	2	142	6	257		M	968					
3	96	5	141	5		8			1293				
4	155	69		145	420	89		1162					
5	100	9		79		6Ø		1113					
6	97	6	194		317	42	Н	1183					
7	92	Ø	140	4	234	5		1180	1228	1263			

Car#:	1 85	•					PC E			Commer	nte. 1	Pup 7	
			•	_	tment	=.7ØF	-/1.ØF	=				160) /	
			BASE	DATA-									
Run#	Date	Drvr	Obsr	Fuel	AirT	Wind	RVP	T29	T2ØA	ACCE.	lerat:	lons-	
								4-0-4		-26	-69	-/9	
1	923	5	15	9	106 93 97 100		1183	1226	1149	99	192	2/1	Т
2	924	5	15	14	93		1475	1986	1100	83	138	192	
3	924	5	15	16	97		1588	1041	1027	95	145	2Ø8	
4	924	5	15	17	100	•	1644	1929	985.	115	167	242	H
5	924	5	15	6	1ø3		1004	1328	1272	92	142	201	T
					91								
7	1004	1	8	15	9,4		1532	1062	1069	93	139	195	Т
8	1004	1	8	16	91 86 85		1588	1Ø41	1Ø69	87	138	189	
9	1012	1	8	в	86	Ť	1124	1258	1321	95	143	207	T
10	1012	1	8	10	85		1242	1195	1265	87	134	194	Т
									HVG:	71.1	141.	ZXIKI.	
					Tmp								
					Air						sec	RSt#	
1					107						4		
6	193	91	123	1Ø1	92	164	115	915	SC	•	2		
	185	93	120	1Ø2	92	163	94	925	SC		2		
					15-								
					Time								
1	78	8	175	24	. 245	23	T	1093	1276	1195			
6	1Ø2	12	15Ø	6.	2Ø8	4	T	15Ø4	1Ø74	1078			
フ	191	110	296	110	. 419	110	L!!	1386	1125	1143			es!!
					CONDIT								
Run#	Smp#	-Tmp	a Sta	art	Tmp	) D Er	1 <b>d</b> .	Avg	Sky	Wind	Sta	rting	
					Air	TcA	TcB	AirT.			sec	RSt#	
1		1Ø7						1070					
2	47	93			93			93Ø					
3	86	97	128					· 97Ø					
4	51	100			100		131		CL				
5	15	103	142	113	1,04	191	119		CL				
6	187	93	122	111	94 93 9ø	163		935					
フ	184	93	124	100	93	171		93Ø					
8	21Ø	91		107	9Ø	162	87		SC				
9	337	86	117		86	176		860	SN				
10	344	85	1Ø9		84	174		845	SN				
					ACCELE								
					15-				T2Ø	T2ØA			
					Time								
1	119	31	207	47	281	41		1045					
2	1Ø1	11	154	9	210	5	Т	1409					
3	96	5	150	6	2Ø2	1				1068			
4	102	12	161	14	227	14		1384					
5	114	25	176	25		22		1013					
6	128	51	189	34	247	24		1352					
7	1Ø3	13	155	10	213	7		1265					
8	1Ø2	12	150	6	2Ø6	3		1428					
9	95	4	146	4	21Ø	5		1188					
1Ø	94	3	142	1	197	-1	T	1303	1164	1238			

		^										•	
C	14	•						(a) D			nts: f	2e	1 8
Car#:	10		Taa- '	\al i 4					ald l		icai I	· CIII	.,0
			Lewb (										
													Surg
	924										183		
	924		15	4	1Ø4		882	1405	1342	125	188	277	
3	924	5	15	6	1Ø7		1004	1328	1244	123	184	268	
4	1004	2	8	6	89		1004	1328	1370	124	179	257	T
5	1005	2	8	4	91		882	14Ø5	1433	127	179 185 189 184	27Ø	T
6	1005	2	8	9	9Ø		1183	1226	1261	131	189	286	T
7	1006	2	8	2	9Ø		759	1488	1523	126	184	277	Т
8	1006	2	8	1	92		697	1532	1553	126	183	272	M
9	1Ø13	2	8	5	89		943	1366	14Ø8	127	184	303	
	1Ø14												
		_		_	<u>.</u>				Ava:	126.	184.	276.	•
			/EV_08	e en	א כטו	IDITI	NG						
	Smp#												
												NO C#	
. 1	22	191	134	126	161	152	154				4		
								. Ø		•			
												•	
- Run#											•		
	Time	%Inc	Time	%Inc	Time	%Inc							
1	132	5	253	38	358	3Ø	M	1140	1249	1207			
		Ø		Ø		Ø			Ø	Ø			
			THE	DAY (	TONE T								
				SUHN I	TONDI	I TONZ-							
Run#											Star	ting	
	Smp#	-Tmp	9 Sta	art	Tmp	a Er	nd	A∨g	Sky	Wind			
~	Smp#	A1r -Tmp	a Sta TcA	rt TcB	Tmp	a Er T.⊂A	nd TcB	Avg AirT	Sky	Wind			
1	Smp#  465	-Tmp A1r 102	9 Sta TcA 136	rt TcB 14Ø	Tmp Air 103	a er T.⊂A 16ø	TcB 164	Avg AirT 1025	Sky  CL	Wind			
1 2	Smp#  465 .468	-Tmp A1r 102 104	9 Sta TcA 136 142	TcB 14Ø 144	Tmp Air 103 105	a er T.cA 16Ø 165	TcB 164 171	Avg AirT 1025 1045	Sky CL CL	Wind			
1 2 3	Smp#  465 .468 6Ø	-Tmo Air 102 104 106	9 Sta TcA 136 142 140	TcB 140 144 143	Tmr Air 103 105	9 Er T.CA 160 165 162	TcB 164 171 168	Avg AirT 1025 1045 1060	Sky CL CL CL	Wind			
1 2 3 4	Smp# 465 .468 6Ø 2Ø3	-Tmp A1r 102 104 106 89	9 Sta TcA 136 142 140 124	TcB 14Ø 144 143 135	Tmr Air 1Ø3 1Ø5 1Ø6 88	0 0 Er TcA 16Ø 165 162 148	TcB 164 171 168 151	Avg AirT 1025 1045 1060 885	Sky CL CL CL SC	Wind			
1 2 3 4 5	Smp#  465 .468 60 203 230	-Tmp Air 102 104 106 89 91	9 Sta TcA 136 142 140 124 127	TcB 140 144 143 135 132	Tmp Air 103 105 106 88 91	7 2 Er TcA 160 165 162 148 152	TcB 164 171 168 151 155	Avg AirT 1025 1045 1060 885 910	Sky CL CL SC SN	Wind			
1 2 3 4 5 6	Smp#  465 .468 .6Ø 2Ø3 23Ø 215	-Tmp Air 102 104 106 89 91	9 Sta TcA 136 142 140 124 127 128	TcB 140 144 143 135 132 138	Tmp Air 103 105 106 88 91	7 CA 160 165 162 148 152 152	TcB 164 171 168 151 155 158	Avg AirT 1025 1045 1060 885 910 910	SKY CL CL SK SKY	Wind			
1 2 3 4 5 6	Smp#  465 .468 .6Ø 2Ø3 23Ø 215	-Tmp Air 102 104 106 89 91	9 Sta TcA 136 142 140 124 127 128	TcB 140 144 143 135 132 138	Tmp Air 103 105 106 88 91	7 CA 160 165 162 148 152 152	TcB 164 171 168 151 155 158 159	Avg AirT 1025 1045 1060 885 910 910 905	2	Wind			
1 2 3 4 5 6 7	Smp# 	-Tmp Air 102 104 106 89 91 91 90	9 Sta TcA 136 142 140 124 127 128	TcB 140 144 143 135 132 138	Tmp Air 103 105 106 88 91	7 CA 160 165 162 148 152 152	TcB 164 171 168 151 155 158 159	Avg AirT 1025 1045 1060 885 910 910 905 920	2 - C C C C C C C C C C C C C C C C C C	Wind			
1 2 3 4 5 6 7 8	Smp# 	-Tmp Air 102 104 106 89 91 91 90 92	7 Sta TcA 136 142 140 124 127 128 124 127 124	TcB 140 144 143 135 132 138 130 132	Tmp Air 103 105 106 88 91 91 91 92 89	7 Per T.CA 169 165 162 152 155 155 157	TcB 164 171 168 151 155 158 159 165	Avg AirT 1025 1045 1060 885 910 910 905 920 890	8 - C C C C C C C C C C C C C C C C C C	Wind			
1 2 3 4 5 6 7 8 9	Smp#  465 468 60 203 230 215 259 259 252 314 339	-Tmp Air 102 104 106 89 91 91 90 92 89	7 Sta TcA 136 142 140 124 127 128 124 127 124 125	TcB 140 144 143 135 132 138 130 132 133	Tmp Air 103 105 106 88 91 91 91 92 89	7 a Er T.CA 165 165 162 148 152 155 155 157	TcB 164 171 168 151 155 158 159 165	Avg AirT 1025 1045 1060 885 910 910 905 920 890 890	8 - C C C C C C C C C C C C C C C C C C	Wind			
1 2 3 4 5 6 7 8 9	Smp#	-Tmp Air 102 104 106 89 91 91 90 92 89	9 Sta TcA 136 142 140 124 127 128 124 127 124 125	TcB 140 144 143 135 132 138 130 133 135	Tmp Air 103 105 106 88 91 91 91 92 89 ACCELE	a Er T.CA 169 165 148 152 155 155 157 149 ERATIO	TcB 164 171 168 151 155 158 159 165 156	Avg AirT 1025 1045 1060 885 910 910 905 920 890	8 - L L C C C S S S S S S S S S S S S S S S	Wind			
1 2 3 4 5 6 7 8 9 10 Run#	Smp#	-Tmp Air 102 104 106 89 91 91 90 92 89	9 Sta TcA 136 142 140 124 127 128 124 127 124 125 IDLE S	TcB 140 144 143 135 132 138 130 132 133 135	Tmp Air 103 105 106 88 91 91 91 92 89 4CCELE	7 0 Er T.CA 169 165 162 152 155 155 157 149 ERATIO	TcB 164 171 168 151 155 158 159 165 159 156 Surg	Avg AirT 1025 1045 1060 885 910 905 920 890 870	8 - L L C C C S S S S S S S S S S S S S S S	Wind			
1 2 3 4 5 6 7 8 9 10 Run#	Smp#	-Tmp Air 102 104 106 89 91 91 92 89 . 89 . 50	9 Sta TcA 136 142 140 124 127 128 127 124 125 Time	TcB 140 144 143 135 132 138 130 133 135 60AK 7-60	Tmp Air 103 105 106 88 91 91 92 89 4CCELE15- Time	9 PER TCA 169 165 162 152 155 155 157 149 ERATIO 70	TcB 164 171 168 151 155 158 159 165 159 156 Surg	Avg AirT 1025 1045 1060 885 910 905 920 890 870	Sky CL CL SC SC SC SC SC SC SC SC SC SC SC SC SC	Wind T2ØA	sec	RSt#	
1 2 3 4 5 6 7 8 9 1ø	Smp#	-Tmp Air 102 104 106 89 91 91 92 89 . 89 . 50 %Inc 3	9 Sta TcA 136 142 140 124 127 128 127 124 125 Time 195	TcB 140 144 143 135 132 138 130 133 135 60AK 7-60	Tmp Air 103 105 106 89 91 91 92 89 4CCELE15- Time >873	7 0 0 Er Tc8 169 162 148 152 155 157 149 ERATIO 70 71nc	TcB 164 171 168 151 155 158 159 165 159 156 NS	Avg AirT 1025 1045 1060 885 910 910 905 920 890 RVP	Sky CL CL CC SN SN SN SN T20 1284	Wind  T2ØA  1232		RSt#	=•!!
1 2 3 4 5 6 7 8 9 10 	Smp#	-Tmp Air 102 104 106 89 91 91 92 89 . 89 . 50	9 Sta TcA 136 142 140 124 127 128 127 124 125 Time	TcB 140 144 143 135 132 138 130 133 135 60AK 7-60	Tmp Air 103 105 106 89 91 91 92 8915 Time >356	9 PER TCA 169 165 162 152 155 155 157 149 ERATIO 70	TcB 164 171 168 151 155 158 159 165 159 165 Surg	Avg AirT 1025 1045 1060 885 910 905 920 890 890 RVP	Sky CL CL CL SN SN SN SN T20 1284 1363	T2ØA  1232 1297	sec	RSt#	=•!!
1 2 3 4 5 6 7 8 9 1ø	Smp#	-Tmp Air 102 104 106 89 91 91 92 89 . 89 . 50 %Inc 3	9 Sta TcA 136 142 140 124 127 128 127 124 125 Time 195	TcB 140 144 143 135 132 138 130 132 133 135 60AK 7	Tmp Air 103 105 106 89 91 91 92 89 4CCELE15- Time >873	2 9 Er Tc69 165 162 148 152 155 157 147 179 nc 79 nc 299 37	TcB 164 171 168 151 155 158 159 165 159 165 Surg	Avg AirT 1025 1045 1060 885 910 910 905 920 890 RVP	Sky CL CL CL SN SN SN SN T20 1284 1363	T2ØA  1232 1297	sec	RSt#	=•!!
1 2 3 4 5 6 7 8 9 10 	Smp#	-Tmp A1r 102 104 106 89 91 92 89 	9 Sta TcA 136 142 140 124 127 128 124 127 125 IDLE S 15- Time 195 194	TcB 140 144 143 135 132 138 130 132 133 135 60AK 2Inc 66	Tmp Air 103 105 106 89 91 91 92 8915 Time >356	7 200 149 149 148 152 155 157 149 170	TcB 164 171 168 151 155 158 159 165 159 165 Surg	Avg AirT 1025 1045 1060 885 910 905 920 890 890 RVP	Sky CL CL CL SN SN SN SN SN 1284 1363 1320	T2ØA  1232 1297 1243	sec	RSt#	=•!!
1 2 3 4 5 6 7 8 9 1ø 	Smp#	-Tmp A1r 102 104 106 89 91 90 92 89	9 Sta TcA 1342 140 124 127 128 124 127 125 10LE S 15- Time 195 194	TcB 140 144 143 135 132 138 130 132 133 135 60AK 7	Tmp Air 103 105 106 88 91 91 92 89 4CCELE15- Time >856 378	2 9 Er Tc69 165 162 148 152 155 157 147 179 nc 79 nc 299 37	TcB 164 171 168 151 155 158 159 165 159 156 NS Surg	Avg AirT 1025 1045 1060 885 910 905 920 890 890 RVP  1078 947	Sky CL CL CL SC SN SN SN SN SN 1284 1363 1320 1178	T2ØA  1232 1297 1243 1224	sec	RSt#	=•!!
1 2 3 4 5 6 7 8 9 1ø 	Smp#	-Tmp A1r 102 104 106 89 91 92 99 	9 Sta Tc36 142 148 124 127 128 127 127 125 174 195 194 208 192 408	TCB 140 144 143 135 132 138 138 138 138 138 135 80AK 6 60A %Inc 69 4	Tmp Air 103 105 105 105 107 107 107 107 107 107 107 107 107 107	7 A Er TCAØ 165 162 148 152 155 157 149 ERATIO 707 717 200 27 33 86	TcB 164 171 168 151 155 158 159 165 159 156 NS Surg	Avg AirT 1025 1045 1060 885 910 905 920 890 890 RVP  1078 947 1018 1275	Sky  CL CL SC SN SN SN SN SN 1284 1363 1320 1178	T2ØA  1232 1297 1243 1224 12Ø7	sec	RSt#	=•!!
1 2 3 4 5 6 7 8 9 10 Run#	Smp#	-Tmp A1r 102 104 106 89 91 90 92 89 %Inc 35 34 4	3 Tc34 142 142 124 127 128 127 127 125 10LE 15 174 200 172 408 179	TCB 140 144 143 135 132 138 133 135 60A %Inc 69 4 122	Tmp Air 103 105 105 105 105 105 105 105 105 105 105	P A Er T C A Ø 1 6 5 2 1 6 5 2 1 5 5 5 5 5 7 1 4 9 7 1 7 8 7 7 7 7 7 7 7 8 8 8 1 Ø 8	TcB 164 171 168 151 155 159 165 159 156 NSurg MMM MHL	Avg AirT 1025 1045 1060 885 910 905 920 890 890 RVP  1078 947 1018 1275 1274	Sky  CL CL SC SN SN SN SN SN 1284 1363 1320 1178 1179	T2ØA  1232 1297 1243 1224 12Ø7 1216	sec	RSt#	=•!!
1 2 3 4 5 6 7 8 9 1ø Run# 1 2 3 4 5	Smp#	-Tmp A172 104 106 89 91 92 89 	3 Tc342 1444 1244 127124 127124 127125 10LE 15- 1944 1944 1991	T-B 144 143 135 132 138 1332 1335 135 600 7 128 4	Tmp Air 103 105 105 105 107 107 107 107 107 107 107 107 107 107	PA ER TC405 1465 148 152 155 157 149 ERATIO 72 108 108 108 108 108 108	TcB 164 171 168 151 155 159 165 159 156 NS MM MH LH	Avg AirT 1025 1045 1060 885 910 920 890 890 RVP 1078 1275 1274 1255 1289	Sky  CL CL CL SC SN SN SN SN 1284 1363 1378 1179 1188 1171	T2ØA 1232 1297 1243 1224 1207 1216 12Ø3	Proxy	RSt#	
1 2 3 4 5 6 7 8 9 1ø Run# 1 2 3 4 5 6 7	Smp#	-Tmp A1r 102 104 106 89 91 92 89 70 70 71 35 34 47 32	9 Tc3420 1440 1241 1271 1281 1271 1271 1271 1271 1271 127	T-B 140 144 143 135 132 138 1332 1335 135 600 7 122 128 40	Tmp 10510568 1189199999999999999999999999999999999	PA ER T.645 1.645 1.648 1.55 1.55 1.55 1.55 1.47 1.70 1.70 1.70 1.70 1.70 1.70 1.70 1.7	TcB 164 171 168 151 155 159 165 159 156 NS MM MH LH	Avg AirT 1025 1045 1060 885 910 920 890 890 RVP 1078 1274 1255 1289 1279	Sky  CL CL SC SN SN SN SN 1284 1363 1178 1179 1188 1171 1176	T20A 1232 1297 1243 1224 1207 1216 1203 1197	sec	RSt#	
1 2 3 4 5 6 7 8 9 1ø Run# 1 2 3 4 5	Smp# -465 .468 .203 .230 .230 .235 .257 .252 .339 15 .1329 .1339 .134 .129 .131	-Tmp A172 104 106 89 91 92 89 	3 Tc342 1424 1221 1221 1221 1221 1221 1221 1	T-B 144 143 135 132 138 1332 1335 135 600 7 128 4	Tmp Air 103 105 105 105 105 105 105 105 105 105 105	PA ER TC405 1465 148 152 155 157 149 ERATIO 72 108 108 108 108 108 108	TcB 164 171 168 151 155 159 165 156 NSurg MM MH LH!!	Avg AirT 1025 1045 1060 885 910 920 890 890 RVP 1078 1274 1255 1289 1279	Sky 	T2ØA  1232 1297 1243 1224 12Ø7 1216 12Ø3 1197 1351	Proxy	RSt#	

		-			 -yur a,		. LU	-~, 171					
Car#:	17								ata (	Conner	nts: N	ło	
					tment								
					AirT						lerati	ons-	Sura
											~-6Ø		
											143		
2	1Ø14	8	1	17	9Ø		1644	1Ø2Ø	1Ø55	110	168	28Ø	
3	1014	8	2	15	9Ø				1Ø97	1Ø9	153	266	
							_	Ø					
			-					Ø					
							Ø	_	-				
							Ø						
							Ø	Ø		1014	158	250	
			<ey-of< td=""><td>FF SO</td><td>AK COM</td><td>DITIO</td><td>)NS</td><td></td><td></td><td>127. </td><td></td><td>237 </td><td></td></ey-of<>	FF SO	AK COM	DITIO	)NS			127. 		237 	
									Sky	Wind	Star	ting	
		Air	TcA	TcB	Air	TCA	T⊂B	AirT			sec		
1	350	9Ø	1Ø1		9Ø 9Ø	124		900	· SN		32	3	
2	372	90	110		9Ø	136		900	SN		19		
3	32Ø	9Ø	111		9Ø	131		900	SN		4		
								Ø					
								Ø					
								Ø					
			/EV. OF		NK 800	·	\ T T C\(\)	Ø					
					9K AC0 15-								
					Time								
					277								
2	125	21	193	22	319	23	•	1627	1026	1061			
3	124	20	189	20	313	21		1510	1Ø71	1106			
		Ø		ø	•	Ø			Ø				
		Ø		· ø		Ø			Ø	Ø			
		Ø				Ø			Ø	· <del>-</del>			
		Ø		Ø		Ø				Ø			
											 Star		
											sec		
		9Ø	105	142	90	127	165	ี่ 9ผผ	SN		366	IVO E W	
2		90	108		9Ø 9Ø	140		900	SN				
3		91	110	•	91	134		910	SN				
								Ø					
								Ø					
								Ø					
		_						Ø					
					ACCELE					T0//A			
					15- Time			RVP	120	T2ØA			
1	1Ø6	2100	162	3 June	273	71nc		1591	1039	1074			
2	131	26			351				1069				
3	126	22	190	20					1101				
•		Ø		ø		ø			ø	ø			
		Ø		Ø		ø			Ø	ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
						-							

										_			
Car#:	18		Temp /	مر نیرون	taant				ata (	Commen	ts: F	un 1	
			BASE										
Run#										Accel			
		_								-5Ø			
1	1006	8	2	17	9Ø		1644 Ø	1020 0	בכיאו פ	76	145	217	
							ži	ø	g				
							Ø	g	ø				
							ęs	ø	Ø				
							<u>Q</u> 1	Ø	Ø				
							gi	Ø	Çi				
							Ø	Ø	Ø				
									Avg:	96	145	217	
			KEY-OF								C+	+ :	
Run#	2mp#									Wind		RST#	
1	282		113				,	895			4	1	
•	204	7 %	***		•			g			•	-	
								Ģ					
								Ø					
								Ø					
								Ø					
			·=> 0		NK 000		\ T T ON!	Ø					
D., p.#			EY-01 15							T200A			
			Time				_						
	103	7			231					1107			
_		ø		Ø		Ø			Ø	Ø			
		Ģi.		gi		Ø			<u> Ç</u> i	Q1			
		Ø		Ø		Ø			Ø	<u>g</u> i			
		ø		g		Q1			ģi ~	Ø			
		Ø		୍ର ଓ କ		Ø			Ø	Ø			
		QI 	TDIE 6	SUVA (	ב אות ב	Ø CTONG-			Ø	ģi 			
										Wind		ting	
			TcA					AirT				RSt#	
1	256		1112		90	124		900	SN				
								Ø					
								Ø					
								Ø G					
								Ø Ø					
								ø					
			IDLE S	SOAK A	ACCELE	RATIO	)NS						
		-50	15-	-60	15-	-70			T2Ø	T2ØA			
			Time										
1	90	-6	131	-10	,217	ø		1617	1030				
		<u>ହ</u>		Ø		Ø			Ø	Ø			
		Q1 Ø		ହା ହା		Ø Ø			Ø Ø	ହ ହ			
		ei ei		ei Ei		gi			gi	gi			
		ģ		ā		Ø			· Ø	Ø			
		Ø		Q1		ø			Q1	Ø			

Car#:	19	•		Temp /	 teut bA					Commer	nts: f	หินภร ส	5,7
			DAGE	DATA.				- / 2 2 20					
Run#	Date	Drvr	Obsr	Fuel	AirT	Wind	RVP	T2Ø	T2ØA	Acce:	lerati	ons-	Surg
1	924	5	15		106								
					90								Т
					91								Ť
<u> </u>	1005	1	٥	11	01		1301	1145	1107	171	206	3₹ <b>4</b>	Ť
7	1/3/3/4	1	0	7	94		1064	1707	1700	104	104	298	
,	1 22/27	•	0		7 k r		407	1270	1546	1/37	170	276	
9	1 (2/2/2)	1	0	1	71		407	1002	150%	197	100	ニアサ	Ť
<u> </u>	1990			,	70		1001	1332	1340	127	170	- C.W.C.	
8	1912	1	8	0	91 9Ø 91 93 85		1994	1028	1078	188	102	277	
4	1912	1	8	ٽ م	84		821	1445	1022	122	185	299	Т
19	1913	1	2	1	85 87		69/	1532	1602	111	178	298	_
11	1913	1	2	2	87		/59			112	172	277	7
											189.		
					AK COM								
Run#	Smp#	-Tmp	a Sta	art	Tmp	o a Er	nd	A∨g	Sky	Wind	Star	ting	
					Air							RSt#	
					1Ø7				CL		2		
					ak ACC								
					15-								
	Time	%Inc	Time	%Inc	Time	%Inc							
1	128	6	212	12	335	11		1177	1229	1149			
			IDLE S	30AK (	CONDIT	TIONS-							
Run#	Smp#	-Tmp	a Sta	art	Tmp	a Er	nd	Avg	Sky	Wind	Star	ting	
					Air								
	24				197								
2		90			9Ø				SN				
3		91	114	129	91	162	167	910	SN				
4	249		113	126	91 91	168		910	SN				
5	26Ø		119	135	90	164			SN				
5	255				92				SN				
- <del>-</del> -		93			93				SN				
3		85			85				SN				
9		84			84		167		SN				
1Ø		05	104	140	94	127							
11	740	85 87	117	140	88 84	177	171	075	SN				
					ACCELE								
					15								
					Time			NVF		1 4 2 7 7			
								1174	1057	11/0			
1	184	52 02	264	39		26		1134					
2	22Ø	82	315	66				1508					
3	219	81	323	71	496	65		1488					
4	199	65	281	48	456	52		1381					
5	199	దర్	283	50	416	38		1258					
6	_				372	24		1272					
7	176	46	254	34	391	30		1258					
8	137	13	232	23	396	32		1988					
9	139	15	223	18	362	29		912					
10	121	ણ	195						1461				
11	129	フ	207	9	339	13	T	826	1442	1495			

Car#:			•	-	tment	=.70	F/1.ØF	=		Commer		No	
	Date	Drvr	Obsr	Fuel	AirT	Wind	RVP	T2Ø	T2ØA	Acce	lerati		
1	928				67								
2		1	5	3	72		821	1445	1431	121	184		
3	928		5	4						12ø			
4				5	7Ø		943	1366	1366	126	188		
5	929		5	6	77		1004						
6		1	5	8	83					124			
		1	5	6	66					128			
8	1012	1	8	7	76		1064	1293		125			T
										124.			
					ak con								
् Run#					Tmp								
					Air						sec	RSt#	•
_	414	67					75				2		
					74			73Ø	SN		3	1	
3	419	8Ø		95	80		92	800	SN		3		
4	107	7Ø	105		71				SN				
. <b>5</b>	12Ø	77			79						2		
6	134	83			83		93				3		
7		66	107	77	66 -	121	· 7Ø	66Ø	SN		2		
8	283	76	116	87	76	134	83	760	SN		2		
		k	CEY-OF	F SOA	AK ACC	ELERA	PLIONS	3					
Run#	15-	·5Ø	15-	-6Ø	15-	7Ø	Surg	RVP	T2Ø	T2ØA			
	Time	%Inc	Time	%Inc	Time	%Inc							
1	13Ø		228		487			1440	1101	1115			
2	- 123	Ø	194		4Ø9	17		933	1372	1351			
3	123	Ø	19Ø	1	383	10	Т	954	1359	1289			
4		-1	185	-1	368	5			1326				
5	127	3	199	75	453	30		1061					
6	122	-1	183	-2	372 51Ø	6		1177					
7	133	8	21Ø	12	510	46		1998	1273	13Ø1			
8	127	3	194	3	451	29	Т	1151	1243	1201			

_				~~									
Car#	: Ø2						CEC E	ו ומני	\	C			
			Temp (	ad ine	++	- 70	CINC 17	CET F	ata	Cowwei	nts: h	Kun 1	
			ם ממם	とという	- menic	/ %	L ( 1 • %)	Г					
Runa	t Date	Deve		DHIH Curl									
7.5077	# Date	Drvr	uosr	ruel	HILÎ	Mruq	RVP	T29	TZØA	Acce:	lerati	ions-	Surg
								~		-50	-60	-70	
	1 1991	4	10	17	73		1644	1920	999.	142		473	
							Ø				- T 24°	77.5	
							ø						
								-					
							Ø	Ø	Ø				
							Ø	Ø	Ø				
							ġ1	્યા	Ø				
							Ø	(3)	Ø				
							ø	Ø					
							·	×.,					
~			/EV_00	E 60	N. 00		20.00		Avg:	142	24Ø	473	
D			\E 1 ~ Ur	.L ani	4K - CUI	MDILI	NN2						
INC.	Smp#	- imp	a Sta	irt	Tm	p a E	nd	Avg	Sky	Wind	Star	tina	
		HIL	ICH	ICE	AIF	TEA	TcB	AirT			sec	RSt#	
1	158	73	75		74	76		735			2		
								Ø			-	•	
								-					
								Ø					
								Ø		•			
								<u> 1</u> 21					
								Ø					
								Ø					
	~~~~	K	EY-OF	F SOA	K ACC	CELERA	TIONS	;					
Run#	15-	-5Ø	15-	60	15-	-70	Sura	DUD	TOG	TOGA			
	Time	%Inc	Time	Toc	Time	7 T	ou. g	LAL	120	, I ZWH			
1	148	4	258	8									
•	170		200		515		ı	1640	1021	997.			
		Ø		Ø		Ø			Ø	Ø			
		હા		Ø		Ø			Ø	Ø			
		Ø											
		**		Ø		Ø			a				
		g g		-					Ø	Ø			
		Ø		Ø		Ø			Ø	Ø Ø			
		Ø Ø		Ø Ø		Ø Ø			Ø Ø	Ø			
		Ø Ø Ø	DI E 04	Ø Ø		@ Ø Ø			Ø Ø Ø	Ø Ø Ø			
		Ø Ø Ø	Dre Si	Ø Ø Ø	TIQNO	Ø Ø Ø 'TONS~		~	Ø Ø Ø	Ø Ø Ø			
Run#	 Smp#	Ø Ø Ø 1	9 -5ta i	Ø Ø Ø DAK C	Tmp	@ @ `IONS~ `∂ En	d	Ava	Ø Ø Skv	@ @ @ @ 	Start	 tina	
Run#		Ø Ø Ø 1	9 -5ta i	Ø Ø Ø DAK C	Tmp	@ @ `IONS~ `∂ En	d	Ava	Ø Ø Skv	@ @ @ @ 	Starf	 ting	
Run#	Smp# 	Ø Ø Ø 1	9 -5ta i	Ø Ø Ø DAK C	Tmp Air	@ @ `IONS~ `∂ En	d	Avg AirT	Ø Ø Ø Sky	Ø Ø Ø	Starf	 ting RSt#	
_		Ø Ø Ø I -Tmp Air	9 -5ta i	Ø Ø Ø DAK C	Tmp	@ @ `IONS~ `∂ En	d	Avg AirT 755	Ø Ø Skv	@ @ @ @ 	Start	 ting RSt#	
_		Ø Ø Ø I -Tmp Air	9 -5ta i	Ø Ø Ø DAK C	Tmp Air	@ @ `IONS~ `∂ En	d	Avg AirT 755 Ø	Ø Ø Ø Sky	@ @ @ @ 	Start	 ting RSt#	
_		Ø Ø Ø I -Tmp Air	9 -5ta i	Ø Ø Ø DAK C	Tmp Air	@ @ `IONS~ `∂ En	d	Avg AirT 755 Ø	Ø Ø Ø Sky	@ @ @ @ 	Start	 ting RSt#	
_		Ø Ø Ø I -Tmp Air	9 -5ta i	Ø Ø Ø DAK C	Tmp Air	@ @ `IONS~ `∂ En	d	Avg AirT 755 Ø Ø	Ø Ø Ø Sky	@ @ @ @ 	Start	 ting RSt#	
_	167	0 0 0 	D-Sta , TcA	Ø Ø Ø DAK C TCB	Tmp Air 76	Ø Ø Ø Ø En Tca	TcB	Avg AirT 755 Ø	Ø Ø Ø Sky	@ @ @ @ 	Start	 ting RSt#	
1	167	0 0 0 	D-Sta TcA DLÈ SO	Ø Ø Ø DAK C TcB	Tmp Air 76	Ø Ø Ø TIONS- D En TCA	d TcB	Avg AirT 755 Ø Ø	Ø Ø Ø Sky	@ @ @ @ 	Start sec F	 ting RSt#	
t Run#	167 	0 0 0 -Tmp Air 75	D-Sta TcA DLÈ SC	DAK C	Tmp Air 76 CCELE	Ø Ø Ø IONS- O Ø En TcA RATIO	d TcB	Avg AirT 755 Ø Ø	Sky	Ø Ø Ø Wind	Start sec F	 ting RSt#	
t Run#	167 167	0 0 0 -Tmp Air 75	D-Sta TcA DLÈ SC	DAK C	Tmp Air 76 CCELE	Ø Ø Ø IONS- O Ø En TcA RATIO	d TcB	Avg AirT 755 Ø Ø Ø	Ø Ø Ø Sky	Ø Ø Ø Wind	Start sec F	 ting RSt#	
t Run#	167	0 0 0 -Tmp Air 75	D-Sta TcA DLÈ SC	DAK A	Tmp Air 76 CCELE 15- Time	OR PORTIONS TO A TO A TO A TO A TO A TO A TO A TO	TcB NS Surg	Avg AirT 755 Ø Ø Ø RVP	Sky SN	Ø Ø Ø Wind	Start sec F	 ting RSt#	
Run#	167 167	0 0 0 	DLE SC Time 7	DAK C TCB	Tmp Air 76 CCELE	RATIO ZUNS-	TcB NS Surg	Avg AirT 755 Ø Ø Ø	8 9 9 Sky SN T20	Ø Ø Ø Wind 	Start sec F	 ting RSt#	
Run#	167 167	0 0 0 	DLE SC Time 7	DAK C TCB	Tmp Air 76 CCELE 15- Time	RATIO ZUNS- TCA TCA RATIO ZUNC ZUNC	TcB NS Surg	Avg AirT 755 Ø Ø Ø RVP	5ky SN T2Ø	720A	Start sec F	 ting RSt#	
Run#	167 167	0 0 0 	DLE SC Time 7	DAK CONTRACTOR	Tmp Air 76 CCELE 15- Time	TIONS- TCA TCA RATIO 70 %Inc Ø	TcB NS Surg	Avg AirT 755 Ø Ø Ø RVP	8 9 9 Sky SN T20	Ø Ø Ø Wind 	Start sec F	 ting RSt#	
Run#	167 167	0 0 0 	DLE SC Time 7	DAK C TCB	Tmp Air 76 CCELE 15- Time	TIONS- TCA RATIO 70 %Inc Ø	TcB NS Surg	Avg AirT 755 Ø Ø Ø RVP	5ky SN T2Ø	720A	Start sec F	 ting RSt#	
Run#	167 167	0 0 0 	DLE SC Time 7	DAK CONTRACTOR	Tmp Air 76 CCELE 15- Time	TIONS- TCA TCA RATIO 70 %Inc Ø	TcB NS Surg	Avg AirT 755 Ø Ø Ø RVP	5ky SN T2Ø 1028 Ø	720A 1518	Start sec F	 ting RSt#	

		•	1702 (N	-yura:								
Car#:	az	•				ــــــــــــــــــــــــــــــــــــــ	באר בי	ial Da	 ata (Commer	nts: N	la	
Carwi	20		Temp 4	ad in et	ment	=. 7ØF			, ,	_ C			
Run#											el ti	mes-	Sura
										-50	-60	-70	
1	922	12	16	14	81		1475	1086			144		
		12	16	17	82						147		
		17	12	17	68		1644	1020	1034	95	137	189	
•							Ø	Ø			_		
							Ø	Ø	Ø				
							Ø	Ø	Ø Ø				
							Ø	Ø	Ø				
							Ø	Ø	Ø				
									Avg:	99	143.	188.	
			KEY-OF	FF 504	AK COM	DITION	INS		_				
Run#	Smp#	-Tmp	a Sta	art	Tmp	_ 9_ Er	nd	Avg	Sky	Wind	Star	ting	
		Air	TcA	TCB	Air	TcA	TcB	AirT			sec	RSt#	
1	500	81	115	1Ø1	83	159	88	82Ø	SNP		1		
2	39	82	124	1Ø4	83	163	9Ø	825	SN		2		
3	2	68	1Ø2	76	48	112	68	680	SC		1		
								Ø					
								Ø					
								Ø					
								Ø					
						CELERA							
						-7Ø							
	Time	%Inc	Time	%Inc	Time	%Inc				4.540			
	111	12	148	4	196	4		1372	1132	1048			
	108	9	153	7	219	12 13		1047	1956	767.			
3	110	11	153	7	212	15		1535	1001	10/5			
		Ø		Ø		Ø				Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø	_	Ø		Ø			Ø Ø	Ø Ø			
			_	_	י מאחי	rions-							
											Star	tina	
		Δi -	Tea	TeR	Air	TeA	TCR	AirT			sec.	RSt#	
		83	121	99	85	142	99	840	SNP				
2	91	85	131		86		101		SN				
3	405	68	1Ø1	73	68	123	72	680	SC				
_								Ø					
								Ø					
								Ø					
		•						Ø					
						ERATIO							
						-7Ø		RVP	T2Ø	T2ØA			
						%Inc	~						
1	106	7	148	4	196	4	_		1132				
2	110	11	151	6	210	12	Т		1079	_			
2	116	17	148	4	2Ø8	11		1527	1064				
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			. Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			

								•					
Car#:	@ 4						CRC F	uel D	ata	Comme	nts: F	kuns	1,5
			Temp	BULDA	tment	=. 7(3)	F/1.	F					
			BASE	DATA									
Fun#	Date	Drvr	Obsr	Fuel	AirT	Wind	RVP	T2Ø	TZØA	Acce	lerati		
1	930	1	15	14	74					146			
2	93Ø	1			78		1444	1474	1275	170	256	461	
3	930	- 1	15	15	90		1670	18/28	704.	130		302	
Ã	1001	•	15	13	989		1552	1962	992.	134	219	33 5	
-	1/3/3/1		15	1/	08		1644	1929	1034	125	197	311	
J	I KIKI I	1	15	17	77		1644	1020	971.	146	223	346	
							Ğ1	Ø	Ø				
							<u>(i</u>)	Ø	Q	ı			
							Ø	Ø	Ø				
									Ava:	130.	204.	316	
			<ey-of< td=""><td>FF 504</td><td>AK COM</td><td>DITIO</td><td>NS</td><td></td><td></td><td></td><td></td><td></td><td></td></ey-of<>	FF 504	AK COM	DITIO	NS						
Run#	Smp#	-Tmp	9 Sta	art	Tmc	a Er	nd	Ava	Sky	ام د داما	Star	+:	-
		Air	TcA	TcB	Air	TCA	Tob	ΔirT		4110	sec sec	CING	
1	103	74		99		135	120	7/5	CN			ドンとお	
2		78	123	106	78		125				3		
3	140	78 8ø	115		90	137		-			3		
4	174	68	1/27	120	OK'	132	122	888	SN			1	
5		77	150	474	78	132	110	685			5	1	
ت	1/4	//	119	121	78	146	116	775	SN		5		
								Ø					
								Ø					
		k	EY-OF	F SOA	K ACC	ELERA	TIONS	3					
Run#	15-	·5ø	15-	·69	15-	70	Sura	RVP	T2Ø	TZØA			
	Time	%Inc	Time	%Inc	Time	%Inc							~
1	157	21	273 279 243 243	34	464	47		1530	1047	1032			
2	156	2Ø	279	37	491	55		1454	1614	074			
3	149	15	243	19	372	-1 0		1654 1577	1-346	70%.			
	144	11	243	19	374	10		1681	12773	7/3.			
5	146	13	278	36	470	77	+	1001	ועשון	16/1/			
_		Ø	2/0	Ø		37	•	16/7					
		ø		Ø		ø Ø			Ø				
			DI			S			Ø	Ø			
	C#	ı	Dre 2	UAK C	ONDII	TON2~	_~~_			*.			
run#	2mp#	_ I WD	a Sta	rt	Imb	9 Eu	d	Avg	Sky	Wind	Start	ting	
		MIL	ICH	ICR	Alr	TCA	TCP	AirT			sec F	RSt#	
	142	/5	116	100	75	128	112	750	SN				
2		78	113	106	79	137	120	785	SN				
3	152	80	114	196	86	136	120	800	SN				
4	199	7Ø	1Ø5	98	72	130	113	710	SN				
5	172	79	112	107	79	143	126	790	SN				
						• -		Ø	<u> </u>				
								ā					
		I	DLE S	DAK A	COELE	PATIO	NG						
Run#	15-	50	15-	40	1 S_	70			T04	TD ~ A			
	Time	%loc	Time :	y toe	Ties '	/ W (our y	RVF	1 210	T2ØA			
1	146	13	246	21	445			4==4					
	144	11				41		1501					
3			243	19		39		1584					
	141	9		13		12		1524					
4	132	2	222	9	359			1657					
5	148	14	256	26	428	35		1618	1029	966.			
		Q1		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			a	a			
NOTES:	Runs	incl	uded i	in bas	se aco	elera	ation	time	AVER	2005	7, 7 4		
R'	VP 15	D 27 X	188	1920 0/	/L & /	iA DYF	r Te	no 2~	a dec	Fx1Ø	, -, - •		
Ac	cceler	ration	n time	s are	gec.	хIØ		m	- 249		,		

Car#:	Ø5					(CRC F	el Da	ata (Commer	its: f	รินตร	1.3
	~~	,	Temp (ad inet	ment								., -
										Accel			Sura
	Date										-60		
		1										_	
	930	1	15	14	70		1475			119	184		
	930	1	15 15 15	17	72		1644	1929	1886	15/	224	313	H
3	930	1	15	15	77		1532	1962	1013	161	227	312	н
4	1001	1	15	16	73		1588	1041	1020	127			Н
5	1001	1	2	14	80		1475	1086	1016	113	178	260	T
							Q 1	Ø	Ø				
							<u> Ç</u> i	Ø	Ø				
							ø	Ø					
									Avg:		181	266	
			/EV_00	e en	אר כטי	unttt	1NS		_				
										Wind		rtina	
				art	i mp	7 - A	7-5	Avg Admit	BKY	MILIO	o Car	CING	
			TcA		Air							KSC#	
	114		131								2		
2	117		134	83	73	17Ø	77	725	SN		6		
3	449	77	142	89	78	176		775	SN		5	1	
4	178	73	127		74	174		735	SN		2		
5	165	8Ø	131	92	81	187	88	8Ø5	SN	•	3		
_								Ø					
								Ø					
			<ey-of< td=""><td>E SO</td><td>אי סכנ</td><td>EL ER</td><td>TTON</td><td></td><td></td><td></td><td></td><td></td><td></td></ey-of<>	E SO	אי סכנ	EL ER	TTON						
			15-										
										1 48/17			
	1100	VIUC.	Time	YTHE	11me	"IUC		1407	1077				
	129	10	191 202 186 223	- 6	2/6	4	M	1497	10//	1873			
2	137	18	2Ø2	12	279	5	Н	1718	994.	977			
3	123	6	186	3	264	-1	Т	1596	1038	985.			
4	164	41	223	23	298	12	Н	1652	1Ø17	993.			•
5	200	72	260	44	331	24	н	1545	1Ø57	984.			
		Ø		Ø		Ø			Ø	Q1			
		gs							(2)	<u>g</u> j			
			IDLE S										
										Wind			
		71		1 4- 2-	71	157	,	710	SN		t t	******	
	118	73	177	04	74	174	04	775	SN				
				90			00			•			
3	197	78	142		78	179		78Ø	SN				
4	161	76	130		76	173		760	SN		_	_	
5	162	81	140	93	82	181	91	815	SN		5	2	
								Ø					
								<i>હ</i> ો					
			IDLE 9										
Run#	15-	·5Ø	15-	-60	15-	-7Ø	Surg	RVP	T2Ø	T2ØA			
	Time	%Inc	Time	%Inc	Time	%Inc							
1	115	-1	184	2	271	2		1479	1984	1077			
2	139	20		_	287	8		1678	-				
3	224	93	288	59	376	41		1520					
4	218	88	280	55´				1627					
5	195	68	258	43	331	24		1498					
3	173		400				F1	1470					
		Ø		Ø		Ø			ğ	Ø			
	_	. Ø		Ø		Ø			Ø	Ģ			
NOTES:													
F	RVP is	, psi	(1ØØ;	Ta2gy	//L &	Avg 6	air Te	emp ar	e de	j Fx18	7;		

Car#:			Temp (=.7ØF	F/1.0W	=		Commer		No	
Run#	Date	Drvr	Obsr	Fuel	AirT	Wind	RVP	T2Ø	TZØA	Acce:	lerat	ions-	Surg
										-50	-60	-70	
Ŧ <u>1</u>	922	1	5				1475	1086	1023	161	159	229	T
2	923	1	5	12	82		1359	1138	1Ø54	111	166	236	
3	927	1	15	14	68		1475	1086	1100	194	160		T
4	927	17	12	17	78		1644	1020	964.	140	2Ø2	281	Н
5	928	1	5	17	78		1644	1020	1020	102	154	22Ø	
6	928	1	5	15	76		1532	1062	1020	99	154	217	T
							<u>Q</u> i	Ø					
							Ø	હ્ય	_		_		
		_	.= ==		==.					102.			
		-								Wind			
			TcA									KST#	
1	451	80		127			89				3 2		
2	40		131	98 74	40	170	89	835			2		
3	421	68 78	11/	/6	- 68 - 70	139 159	/2		SC	•	2 2		
4	446	78	133	86	78	139	82	78Ø					
5		70	11/	81	/1	159	/8	705	SN	•	3 4		
6	422	76	122	9Ø	78	169	8/		SN		4	1	
			<ey-of< td=""><td>E CO</td><td>V ACC</td><td></td><td>\ T T (7 N)</td><td>gi </td><td></td><td></td><td></td><td></td><td></td></ey-of<>	E CO	V ACC		\ T T (7 N)	gi 					
			15										
			Time										
	135	41UC	101	71UC	250	4111		1707	1122	1045			
	1/14	44	202	22 70	230	27	77 LJ	1304	1122	1077			
2 3	140	44	191 2 9 3 166	- SIP	2/4	- 44	M	1470	1805	1800			
4	120	10	180	15	201	7	- H	14/0	1000	1 K/77			
5			202										
6		17	177	47	200	4		1501	1002	004			
G.	117	ø	1//			ø		1001		g, g			
			IDLE 9										
										Wind		rtina	
			139										
2		85				165		860	SN				
			119										
4	450	79	133		8Ø			795	SC				
5	418	71	120		72	151	83	715	SN				
6	61	78	135		79		91	785	SN				
								Ø					
			IDLE S	SOAK A	CCELE	ERATIC	NS						
			15-						T2Ø	T2ØA			
			Time										
1	113	11	176	12	254	13		1355					
2	107	5	175	12	254			1336					
3	102	Ø			230			1472					
4	114	12			249			1605					
5	100	-1	157		214			1585					
6	110	8	174	11	239		Н	1533					
	_	Ø		Ø.		Ø			Ø	ଣ			
NOTES:												5,6	
							ar Te	emp ar	e ded	g Fx19	2 ;		
f	-CC616	erati(on tim	nes ar	-6 260	×1%							

		•	1982 (LKL KE	egular	vapo	or Loc	:K, CC	201				
Car#-	017					۰	יפר בי	e l Da	a+a (്വതരങ	ste: F	200 S	
Car # :	**/	-	Tamo i	اعتناك	ment								
~ ~ ~ ~ ~ ~													
Run#	Date	Dryr	Obsc	Fuel	AirT	Wind	RVP	T20	T2ØA	Accel	lerati	ons-	Sura
										-50	-60		
1	928	17	12	17	70		1644	1020				252	
													М
													Т
•		• •	٠										
							-						
										115.	176.	256	
			CEY-OF	FF SO	AK CON	DITIO	NS						
	1 928 17 12 17 70 1644 1020 1020 112 179 252 2 928 17 12 15 78 1532 1062 1026 126 194 267 3 929 17 12 14 69 1475 1086 1093 112 175 256 4 929 17 12 15 79 1532 10862 999. 118 179 268 5 930 17 16 17 65 1644 1020 1055 130 183 278 6 1012 17 7 12 75 1359 1138 1103 110 172 248 6 1012 17 7 12 75 1359 1138 1103 110 172 248												
1													
	## Date Dryr Obsr Fuel AirT Wind RVF T20 T20A Accelerations—Sure 1 928 17 12 17 70 1644 1020 1020 119 179 252 2 928 17 12 15 78 1532 1062 1006 126 194 267 3 929 17 12 14 69 1475 1006 1093 112 175 256 4 929 17 12 15 79 1532 1062 999 118 179 268 5 930 17 16 17 65 1644 1020 1025 130 183 278 6 1012 17 7 12 75 1359 1138 1103 110 172 248 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0												
			98	76	71	135	75	705					
			108	84	80	150	86	800					
			97	79	65	130	68	650					
			, ,	,									
_											_		
			EY-OF	FF 504	AK ACC	ELERA	TIONS	3					
			246	40	33Ø	29	н	1642	1Ø21	1014			
			209	19	308	20	н	1583	1042	972.			
	122	6	194	1 gi	269	5	Ŧ	1513	1070	1067			
	135	18	197	12	279	9	M	1573	1046	976.			
5		44	230	3 0	340	33	M	1676	1009	1644			
6			2Ø6	17	294	15	. M	1381	1127	1985			
		Ø		Ø		<u> g</u> s			Ø	্র			
			IDLE S	SOAK (CONDIT	IONS-							
Ru <u>n</u> #	Smp#	-Tmp	a Sta	art	Tmp	ia) Er	nd	Avg	Sky	Wind	Star	ting	
		Air									sec	RSE#	
		Temp Adjustment =.70F/1.0F Temp Adjustment =.70F/1.0F BASE DATA											
-2	427	80	118	96	8Ø	158	96	800	SN				
3	119			81	72	128	81						
5			99	74		119	73						
6	269	77			77				SN				
				_									
									T2Ø	T2ØA			
				44	332								
4					32Ø	25	<u> </u>	1521	18/67	786.			
5	115	Ø											
6			202	15		7-		1374	1131				
	_	Ø.		Ø		Ø			63				
NOTES:												4,6	
					//L &		ar Te	emp ar	e deg	3 FX18	7 \$		
•	+CC#16	アスてン	on tin	nes ar	.6 26C	.×16							

```
1982 CRC Regular Vapor Lock, Cool
                                 CRC Fuel Data Comments: No
Car#: 08
              Temp Adjustment = .70F/1.0F
         ----- BASE DATA------
 Run# Date Drvr Obsr Fuel AirT Wind RVP T20 T20A Accelerations- Surg
                         ---- ---- ---- ---- -50 -60 -70 ----
   1 928 4 10 17 79 1644 1020 957.
                                                  88 128 196
                                     Ø
                                          Ø
                                     Ø
                                          Ø
                                     Ø
                                          Ø
                                     Ģ1
                                          Ø
                                                   88 128 196
                                            Avg:
   ------KEY-OFF SOAK CONDITIONS------
 Run# Smp# -Tmp @ Start-- --Tmp @ End--- Avg Sky Wind Starting
   ----
           Air TcA TcB Air TcA TcB AirT
                                            ---
                                                       sec RSt#
   1 428
            79
                           80
                                        795
                                             SN
                                          Ø
    -----KEY-OFF SUAK ACCELERATIONS-----
 Run# --15-50-- --15-60-- --15-70-- Surg RVP T20 T20A
 ---- Time %Inc Time %Inc Time %Inc ---- ----
             1 131 2 197
                                       1622 1028 962.
     89
                               1
             Ø
                       Ø
                                               Ø
             Ø
                       Ø
                                Ø
             Ø
                       Ø
                                Ø
                                               Ø
             Ģ١
                       Ø
                                               (2)
             Ø
   ------IDLE SOAK CONDITIONS-----
 Run# Smp# -Tmp @ Start-- --Tmp @ End--- Avg Sky Wind Starting ---- Air TcA TcB Air TcA TcB AirT --- sec RSt#
   1 441
           89
                          80
                                        800
                                             SN
                                          Ø
                                          Ø
       -----IDLE SOAK ACCELERATIONS----
 Run# --15-50-- --15-60-- --15-70-- Surg RVP T20 T20A
 ---- Time %Inc Time %Inc Time %Inc ---- ----
       82
            -7
               122
                    -5 185 -6
                                       1546 1057
             Ø
                       Ø
                                Ø
                                                    (2)
                                               Ø
             Ø
                                               Ø
                       Ø
                                Ø
                                                    Ø
NOTES: Runs included in base acceleration time averages: All
```

RVP is psix100; T020V/L & Avg Air Temp are deg Fx10;

Acceleration times are sec.x10

```
CRC Fuel Data Comments: Runs 3,6
Car#: 9
                   Temp Adjustment = .70F/1.0F
       ----- BASE DATA----
Run# Date Drvr Obsr Fuel AirT Wind RVP T20 T20A Accelerations- Surg
      ---- ---- ---- ---- ---- ×100 ×10 ×10 "-50 "-60 "-70 --
                                                  163 263
                                   1359 1138 1131
      927
            17
                 12
                      12
                           71
                                                            470
                     9
                                   1183 1226 1177
      927
            17
                 12
                           77
                                                   138
                                                       213
                                                            382
   3
      928
            17
                 12
                       8
                          67
                                   1124 1258 1279
                                                  140
                                                       221
                                                            399
                           74
                                                       203
   4
      928
            17
                 12
                                   1004 1328 1300
                                                  122
                                                            358
   5
                                   882 1405 1321
      928
                 12
                           82
                                                  129
                                                       2Ø7
                                                            346
            17
                                   882 1405 1377
      929
            17
                 12
                           74
                                                   113 190
                                                            363
   6
      929
                                   759 1488 1397
            17
                 12
                           83
                                                  126
                                                       202
                                                            339
                                               Ø
                                                  131 209. 365.
                                             Avg:
      -----KEY-OFF SOAK CONDITIONS-----
Run# Smp# -Tmp @ Start-- --Tmp @ End--- Avg Sky Wind Starting
                                                       sec RSt#
           Air
               TcA TcB Air
                               TCA TCB AirT
                     92
                           72
                                   114
                                        715
                                            SC
      429
            71
                100
                              136
                                        775
      443
                                            SC
            77
                119
                     102
                           78
                              141
                                   126
      423
            68
                 89
                      84
                           69
                              133
                                   112
                                        685
      409
                 97
                      91
                           75
                              141
                                   121
                                             SN
                      98
                              144
      442
                 99
                           82
                                   127
                                        82Ø
            82
                                             SN
      121
            75
                 93
                      89
                           77
                              141
                                   118
                                       760
                                            SN
            83 1Ø5
                    98
                                   126
                           83
                              145
                                         83Ø SC
      -----KEY-OFF SOAK ACCELERATIONS-----
Run# --15-50-- --15-60-- --15-70-- Surg RVP T20 T20A
      sec %Inc sec %Inc sec %Inc ---- x100 x10 x10
                    106 650 78 H 1390 1123 1113
      336 156
               430
                      96 628
                                72
                                     H 1254 1189 1136
      150
            15
                410
                      34 442
                                     H 1222 1205 1216
      200
            53
                28Ø
                                21
      193
            47
                275
                      31 440
                                    H 1101 1271 1240
                                21
   5
      158
            21
                231
                      10 400
                                10
                                   M 964 1353 1269
                237
                         440
                                     T 95Ø 1361 1319
      152
            16
                      13
                                21
      140
             7
                220
                      5
                          363
                                     843 1431 1340
                                 Ø
      -----IDLE SOAK CONDITIONS----
Run# Smp# -Tmp @ Start-- --Tmp @ End--- Avg
                                             Sky Wind Starting
 ---- ---
           Air
               TcA TcB Air
                               TcA TcB AirT
                                                       sec RSt#
            72
               1Ø2
                              124
                                         725
      431
                     96
                           73
                                   111
                                            SC
      448
            78
               112
                    104
                           78
                              133
                                   122
                                        78Ø
      410
            70
                91
                      84
                           70
                              121
                                   114
                                         700
      424
                      93
                           77
                              125
            76
               100
                                   119
                                         765
                                   133
   5
      440
                     1Ø1
            81
                1Ø3
                           81
                              139
                                         810
                           79
      129
                95
                      92
            77
                               116
                                   112
                                         78ø
               1Ø8
      191
            83
                      99
                           84
                              129
                                   123
                                        835
      -----IDLE SOAK ACCELERATIONS------
Run# --15-50-- --15-60-- --15-70-- Surg RVP T20 T20A
      sec %Inc sec %Inc sec %Inc ---- ×100 ×10 ×10
                                   H 1388 1124 1107
      183
            40
               372
                      78
                         558 53
      150
            15
               340
                      63
                         490
                                34
                                     H 1236 1198 1142
      145
                226
                      8
                                     T 1206 1214 1214
            11
      141
             8
                213
                       2
                         370
                                        1083 1282 1236
                                 1
   5
      159
                         395
                                     H 959 1356 1279
                240
                      15
            21
                                 8
      136
                215
                          390
                                 7
                                         944 1365 1309
             4
      142
             8
                223
                          345
                                 17
                                         837 1435 1340
NOTES: Runs included in base acceleration time averages: 2,3,4,5,7
    RVP is psix100; T020V/L & Avg Air Temp are deg Fx10;
```

Acceleration times are sec.x10

Car#:			•	_	tment	=.798	F/1.68	-		Commer	nts:	Yo	
		Drvr	Obsr	Fuel	AirT	Wind	RYP	T2Ø	T2ØA	Acce!	lerat: "-60	ions- "-70	Surg
1	927	. д	10	14	75					115			
2	927		10							106			
3	928		10					1165					
4			19		75			1195					
5		4			81		1964					_	
6		4			69		821				148	226	
7	929	4	169	5	89			1366			149	230	
8	1012	2	8	12	71 8Ø		1359	1138	1131	89	133	2Ø2	Т
9	1912	2	8	3	8Ø		821	1445	1375	92	136	197	T
										97.9		216.	
			(EY-OF	FF SO	AK CON	DITIO	JNS						
Run#	Smp#	-Tmp	a Sta	art	~-Tmp	a Er	nd	Avg	Sky	Wind	Star	ting	
		Air	TcA	TcB			T⊂B	AirT			sec	RSt#	
1	435	75		103	75	123	1Ø7	75Ø	SC		2		
2	432	78	125	110	78 7ø 76	133	113	780			2		
3	62	79	118	1Ø1	7Ø	130	1Ø4	700			4		
4	63	75	119	1Ø5	76	140	115	755			2 2 2 2 2		
5	433	81	131		82	142	122	815	SN		2		
6	148	69	112	94	70	127	1Ø4	695	SN		2		
7	113	8Ø	121	1Ø3	82		1Ø6	810	SC		2		
8		72	99	96	72		95	72Ø			2		
9		8Ø	111	197		135	111				2		
		h	(EY-OF	FF 50/	AK ACC	ELERA	ATIONS	3					
Run#	15-	-5ø	,15-	-6Ø	~-15-	-70	Surg	RVP	T2Ø	TZØA			
					sec								
1	262	168	318		425		Н						
2	133	36	2Ø5	44			M						
3	145	48	182	28	264	22	M	1353	1140	1140			
4	115	19	168		269	25		1327	1153	1114			
5	168	72	213		269 311 248 26Ø	44	Н	1152	1243	1162			
6	110	12	159	12	248	15		965	1352	1356			
·7	119		174	22	260	2Ø		1030	1313	- 1236			
9		-3	136	-5	207	-4	T	1389	1124	$111\emptyset$			
9	102	4	150	5	227	5	Т	924	1378	1268			

Car#:		•								C			
					tment	=.70F	71.0	=		Commer	יובאו	uns .	<i>ک</i> و ا
Run#	Date	Drvr	Obsr	Fuel	AirT	Wind	RVP	T2Ø	T2ØA	Accel -50	lerati -60		Surg
	930	12								153			
ž	930	12	21	12	74		1350	1178	1110	172	278		
Ī		17	21		70		1107	1774	1170	172 157 141 146 138	270		
	708	17	Z1	7	70		1100	1220	11/9	10/	251		_
4	930	1/	21	6	/9		1004	1328	1265	141	22Ø		T
	1001	21	11	3	69		821	1445	1452	146	229	339	
5	1001	21	11	5	79		943	1366	1303	138	218	319	
							Ø	Ø	Ø				
							<u>Ø</u> s	Ø	Ø				
									_	142.	222.	326	
Run#	Տոբ#	-Tmp	a Sta	art	Tmp	o D Er	d	· Avg	Sky	Wind	Star	ting	
		Air	TcA	TcB	Air	TcA	T⊂B	AirT			sec_	RSt#	
1	144	70			71			7.05			1		
2			1Ø7			177					1		
3	145	78				187					i		
4		79		116	90	190	177	705	SN		1		
				110	72	178	102	773	214				
5	192	79	112	194	/2	180	123	/10	SN		1		
6	156	79	114	113	79	191	140	79Ø	SN		2		
								Ø					
						ELERA							
Run#	15-	-50	15-	-6g	15-	-70	Surg	RVP	T2Ø	T2ØA			
	Time	%Inc	Time	%Inc	Time	%Inc							
1	179	2Ø	338	52	625	92	T	1479	1Ø84	1981			
2	153	8	261	17	639	96 71 52 21	Т	1414	1112	1081			
3	198	40	338	52	558	71		1359	1138	1082			
4	1.41	14	275	24	495	52	τ	1140	1270	1177			
5	154	10	270	21	704	21	Ť	01/3	1707	1700			
	100	1 %	27%	21	400	21	<u> </u>	7186	100/	100%			
6	155	g	20%	40	47%	5ø	,	1.024	1010	1200			
				יע מאר מ		Ø CONC.			121	<u> Ç</u> i			
5		J	DLE	SUAK L	ו בעאט,	エロいタン							
KUN#	2mp#	_ iTub	A 255	art	i wb	ו או בע	d	AVG	SKY.	Wind	Star	ting	
		A1 F	ICA	ICE	AIF	ICA	ICH.	Mrt			sec	RSt#	
1	141	71		197	71	146	130	719	SN				
2		75		113	75	146	145		SN				
3	125	78	111	116	78	149	149	78Ø	SN				
4	164	80	115	120	80	15Ø	151	800	SN				
ัร	195	73	107	114	73	145	144	730					
6	181	81	1Ø8	115	81	152		810	SN				
_								Ø	,				
		I	DLE S	OAK A	CCELE	RATIO	NS						
						70				TZØA			
						%Inc							
1	150	6	249	12	395	21			1093	1084			
2	161	14			410				1118				
ŝ	161	14							1149				
4	149	5	235		358 300	1							
		5 5	47 2	6	947 740	7	***	1142	1248	11/8			
5	149								1398				
6	137	-3	211		305			1929	1313				
	_	Ø	_	Ø		Ø			(2)	<u>Ģ</u> I			
NOTES:	Rung	incl	uded	in ba	se ac	celer	ation	time	aver	ages:	4,5,	6	
							ir Te	mp ar	.e qed	Fx 10	•		
A	ccele	ratio	n tim	nes ar	e sec	.×1Ø							

Car#:	12						CRC FL		ata (Commer	nts: 1	Vo	
							F/1.ØF					•	
												·	
							RVP						Surg
	927		12	17	7/		1644	1070	002	1 (3/3	-6Ø	298	
	1012						1644						
4 7	1012	17	, ,	1.4	70		1475	1000	10023	98	138	186	
Δ	10112	17	7	11	. , , 80		1301	1165	1095	94	136	188	
5	1017	17	7	101	68		1242	1195	1209	88	136	182	
5	1013	17	7	11	74		1475 13Ø1 1242 13Ø1 1359	1165	1137	86	132	180	
7	1613	17	7	12	80		1359	1138	1968	90	142	184	
·			•				<u>@</u> I	Ø	Ø				
									Avg:	89.3	137.	184.	
~							ONS						
Run#	Smp#	-Tmp	a Sta	art	Tmp	o DEr	br	Avg	Sky	Wind	Star	ting	•
		Air	TcA	TCB	Air	TCA	TcB	AirT			sec	RSt#	
1	4 <i>9</i> 1€	74	126	98	75	153	90	745	SC		1		
2	271	71	123	99	72	141	107	715	SN		1		
								<u>@</u>					
								Ø					
								Ø					
								Ø					
							. 	Ø					
							ATIONS						
							Surg						
	1004	71DC	150	7.1nc	210	10		1600	1077	1002			
2	1 0 P	10	147	ΙΟ	217	1 4		1641	1021	1010			
	70	Ø	172	g		g		1041	g				
		g		g		ø			ø	Ø			
		g		g		ø			ģi.				
		ø		g		Ø			Ø				
		Ø		ĢI		Ø			ø	গ্ৰ			
							nd						
							TCB				sec	RSt#	
1		75	131	102	75	151	111 128	755	SC				
2	299												
3	270	80	120	113	88	157	140	800	SN				
4	272	81	124		82	159		815	SN				
5	313	69	116		79	158		695	SN				
6 7	3Ø2 3Ø5	75	121 118	108 109	76 81	156 156	142 148	760 810-					
7		84					7 7 7 1 SNS				•		
Run#	15-							RVP	T2Ø	T2ØA			
					Time								
1	100	12	152	11	210	14		1566	1Ø49	1010			
2	98	10	144	5	286	55	Н	1618	1029	998.			
3	92	3	138	1	314	79	Н	1528	1964	994.			
4	100	12	148	8		33	M	1379					
5	86	-4	136	Ģ	198	2			1157				
6	92	3	140	2	188	2			1130				
7	_	-1	138		282	53		1413					
NOTES													
		•				_	Air Te	emp ar	e de	3 F×19) ;		
1	Accele	erati(on tir	nes ar	re sec	.×1Ø							

1982 CRC Regular Vapor Lock, Cool CRC Fuel Data Comments: Run 1 Car#: 13 Temp Adjustment = .70F/1.0F ---- BASE DATA-----Run# Date Drvr Obsr Fuel AirT Wind RVP T20 T20A Accelerations- Surg -50 -60 -70 ----1644 1020 1090 87 129 191 1 927 17 681 10 Ø Ø Ø Avg: 87 129 191 -----KEY-OFF SOAK CONDITIONS-----Run# Smp# -Tmp @ Start-- --Tmp @ End--- Avg Sky Wind Starting Air TCA TCB Air TCA TCB AirT --- ---- sec RSt# 1 494 68 68 76 68Ø SC -----KEY-OFF SOAK ACCELERATIONS----Run# --15-50-- --15-60-- --15-70-- Surg RVP T20 T20A ---- Time %Inc Time %Inc Time %Inc ----193 T. 1561 1Ø51 1Ø65 1 87 Ø 133 3 1 Ø Ø Ø Ü Ģ Q) Ø Ø Ø Ø Ø --IDLE SOAK CONDITIONS-----Run# Smp# -Tmp @ Start-- -- imp @ End--- Avg Sky Wina Starting Air TCA TCB Air TCA TCB AirT sec RSt# SC 1 496 68 68 680 -----IDLE SOAK ACCELERATIONS-----Run# --15-50-- --15-60-- --15-70-- Surg RVP T20 T20A ---- Time %Inc Time %Inc Time %Inc ---- ----

NOTES: Runs included in base acceleration time averages: All RVP is psix100; T020V/L & Avg Air Temp are deg Fx10; Acceleration times are sec.x10

9

5 209

Ø

Ø

1 90

3

Ø

Ø

Ø

136

M 1579 1Ø44 1534

Ø

a

Car#:			Temp			=.70		=				Vο	
Run#	Date	Drvr	BASE Obsr	Fuel	AirT	Wind	RVP	T2Ø	T2ØA	Acce:	lerat:		
1	927				71		1417						
2		4	10	16	77		1588						н
3	927	Т	1Ø 1Ø	1.4	70		1475						- 11
4	74/	- T	10	1.7	40		1475						M
5	720	4	19	14	77							219	M T
2	748	4	16	12	12		1532			55	127	217	,
							Ø						
							<i>Q</i> 3	Ø G	Ģi ~				
							Ø	Ø					
		_								92.3			
			KEY-OF										
			a Sta										
			TCA	TCB	Air	TCA	TCB	AirT					
	403						133				3		
2	27	77	184	130	78	191	147	775	SC		3		
								Q1					
								Ø					
								Ø					
								Ø					
•								Ø					
			KEY-OF	FF SOA	AK AC	CELER	PLIONS	3					
Run#	15-	-50	15-	-6Ø	15-	-70	Surg	RVP	T2Ø	T2ØA			
	sec		sec										
1	88	-5	134	-2	22Ø	-5		1489	1080	1070			
2	130	41	134 218	60	323	40	Н	1633	1024	971.			
		Ø		Ø		Ø			Ø	ହ			
		Ø		Ø		Ø			Ø	Q)			
		<u>@</u>		Ø		Ø			gr-	Ø			
		Ø		Ø		Ø			10	Ø1			
		Ø		Ø		Ø			Ø	ģ			
			IDLE S	BOAK C	CIDNOI	IQNS-							
			9 Sta									ting	
-			TcA									RSt#	
1			15Ø				120						
-			152		78		=	780	SC				
3	438	79	162	125	8ø	166	129	795	SC	•			
4	461	68	144	106	69	162	120	685					
5	497	72	154	118	72	170	131	720	SN				
_						- •		Ø					
							•	ø					
			IDLE S	BOAK A	CCELE	RATIO)NS						
Զ ևп#	15-		15-						T20	T2ØA			
			sec							×19			
1	94	2	139	2	247	7			1085				
ż	103	12	325		441	91		1594					
3	105	14	308		409			1517					
4	95	3	141		246	7		1535					
5	94	2	140	3	306			1592					
J	7.4	ø	4 TK	ø		Ø	11	. w / ~	Ø	8			
		ହ		Ø Ø		ø			Ø	g)			
NOTES:	Rune	-	Ludad	_	150		-a+i	time			1.3	4.5	
			(100;									., -	

1982 CRC Regular Vapor Lock, Cool ______ CRC Fuel Data Comments: Run 1 Car#: 15 Temp Adjustment =. 70F/1.0F ----- BASE DATA-----Run# Date Drvr Obsr Fuel AirT Wind RVP T20 T20A Accelerations- Surg ---- ---- ---- -50 -60 -70 ----88 139 191 1644 1020 1055 65 Ø 88 139 191 Avg: -----KEY-OFF SOAK CONDITIONS-----Run# Smp# -Tmp @_Start-- --Tmp @ End--- _Avg Sky Wind Starting --- -=- sec RSt# ---- Air TcA TcB Air' (cA TcB AirT 1 136 65 119 65 136 650 SN -----KEY-OFF SOAK ACCELERATIONS--Run# --15-50-- --15-60-- --15-70-- Surg RVP T20 T20A ---- Time %Inc Time %Inc Time %Inc ---- ----79 -10 130 -6 185 -3 1672 1010 1045 Ø Ø Ø Ø Ø 0 Ø Ø Ø Ø -----IDLE SOAK CONDITIONS---Run# Smp# -Tmp @ Start-- -- Tmp @ End--- #vg Sky Wind Starting --- Air TcA TcB Air TcA TcB AirT 1 127 66 125 66 139 660 sec RSt# SN -----IDLE SOAK ACCELERATIONS---Run# --15-50-- --15-60-- --15-70-- Surg RVP T20 T20A ---- Time %Inc Time %Inc Time %Inc ----1652 1017 1045 83 -6 13Ø -6 183 -4 Ø Ø Ø Ø Ø NOTES: Runs included in base acceleration time averages: All

RVP is psix100; T020V/L & Avg Air Temp are deg Fx10;

Acceleration times are sec. x10

•			1702 (JAC RE	adar er			-					
Car#:	16						CRC Fu	iel Da	ata (Commer	nts: N	40	
200, 114		-	Temp /	ad iust	tment								
Run#	Date	Drvr	Obsr	Fuel	AirT	Wind	RVF	T2Ø	T2ØA	Accel	lerati	ons-	Surg
	~										-60		
1	928	5	15							116			
2	929	5	15	11	73		13Ø1	1165	1144	113	173	261	
3	929	5	15				1359				166	259	
4	93Ø	5	15	12	65		1359	1138	1173	114	172		
5	93Ø	5	15	14	68		1475	1086	1100	113			
6	930	5	15	16	71		1588	1Ø41	1Ø34	122	179	274	
							Ģi						
							Ø	Ø	Ø				
										115	173.	269	
					ak con								
Run#										Wind			
												RSt#	
1	417	82	113	121	81	136	137	815	SN		2		
								Ø					
								Ø					
								Ø					
								Ø					
								ساني					
								Ø					
					AK ACC								
					15-					T2ØA			
					Time								
1	125	9	37Ø	114	477	77	·H	1443	1100	1019			
		Ø		Ø		Ø			Ø				
		Q1		Ø		Ø				Ø			
		Ø		Ø		Ø			Ø				
		Ø		Ø		Ø			Ø				
		Ø		Ø		Ø			Ø				
		Ø		Ø		Ø			Ø	· -			
										Wind			
											56 C	RSt#	
	139	81	113	121	82	148	155	815	SN				
	147		1Ø5		76	131	137	75Ø	SN				
3	132	82	113		83	138	144	825	SC				
4	133	65	98	102	65	119		650					
5	102	68	103			122							
6	116	71	108	112	72	128	130	715	SN				
			7 D	300			anc.	Ø.					
					ACCELE					T744			
					15- Time			7VF	1 2 27	1 Z X/H			
	132	71nc	11 me		796	196		1404	1117	1074			
1 2	122			8 8		190				1092			
3	120		188					1399					
4	117					43				1146			
5	117									1066			
6	114					42		1645					
•	* * 4	_1 Ø		Ø		7 £	1-1	1070	12.75	I E/E/7			
NOTES	Rune						ration	, time			A11		
										Fx18			
•								···-		~	•		

1982 CRC Regular Vapor Lock, Cool CRC Fuel Data Comments: Run 1 Car#: 17 Temp Adjustment =.70F/1.0F --- BASE DATA-----Run# Date Drvr Obsr Fuel AirT Wind RVP T20 T20A Accelerations- Surg ---- ---- ×100 ×10 ×10 "-50 "-60 "-70 ----1644 1020 992. 120 188 302 74 17 10 Ø Ø Ø Ø Ø 120 188 302 Avg: -----KEY-OFF SOAK CONDITIONS-----Run# Smp# -Tmp @ Start-- --Tmp @ End--- Avg Sky Wind Air TCA TCB Air TCA TCB AirT sec RSt# SN 74 76 750 135 1 ----KEY-OFF SOAK ACCELERATIONS----Run# --15-50-- --15-60-- --15-70-- Surg RVP T20 T20A sec %Inc sec %Inc sec %Inc --- x100 x10 x10 203 8 330 9 1638 1022 987. 129 8 Ø Ø Ø Q1 Ø Ø Ø Ø Ø Ø Ø Ø Ø ø --IDLE SOAK CONDITIONS------Run# Smp# -Tmp @ Start-- --Tmp @ End--- Avg Sky Wind Air TcA TcB Air TcA TcB AirT ~~~ 1 137 77 106 79 114 78Ø SN -----IDLE SOAK ACCELERATIONS----Run# --15-50-- --15-60-- --15-70-- Surg RVP T20 T20A sec %Inc sec %Inc sec %Inc --- x100 x10 x10 1 121 Ø 187 -1 295 -1 1611 1032 976. Ø Ø Ø

Car#:1	8				tment	=.7ØF	7/1.ØF	=	ata (Commen	ts: Y	'es	
Run#	Date				AirT				T2ØA	Accel			_
										-50			
1	93Ø	4	1Ø	17	78		1644	1020	964.	1Ø2	153	237	
							Ø	Ø	Ø				
							Ø	Ø	Ø				
							Ø	Ø	Ø				
							Ø	Ø					
							Ø	Ø	Ø				
							Ø	Q1	Ø				
							Ø	Ø	Ø				
										102	153	237	_
					ak cov								
										Wind		_	
			TcA	TcB	Air	TcA	TcB				sec	RSt#	
1	1,11	78			78			78Ø	SN				
								Ø					
								Ø					
								Ø		•			
								Ø					
								Ø					
								Ø					
					K YCC								
					15-		_		T2Ø	T2ØA			
					Time								
1	110	8		7	247	4		1438	11Ø2				
		Ø	•	Ø		Ø			Ø	Ø			
		Ø		Q1		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	છ			
												-	
Run#	Smp#									Wind		ting	
		Air	TCA	TcB	Air	TCA	TCB					RSt#	
1	163	78			78			78Ø	SN		4	1	
								Ø					
								Ø					
								Ø					
								Ø					
								Ø					
								Ø					
					JCCETE								
					15-			RVP	T2Ø	T2ØA			
					Time	_							
1	1Ø7	5	161	5	249	5		1459	1093				
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	Q1			
	_	Ø	_	Ø		Ø			121	Ģī			
NOTES	Runs	100	luded	in be	S# AC	celer	ation	, time	e aver	ages:	All		

RUP is psix100; T020V/L & Avg Air Temp are deg Fx10;

Acceleration times are sec.x10

]	1982 (JRU RE	egular 	Vapo	or Loc	ck, Co	201				
Car#:	19					C	ORC F	el Da	ata (Conner	nts: F	Runs 3	2.6
	_		-	Temp A	ad just								•
Run#	Date	Drvr	Obsr	Fuel	AirT								
										Per. 10.			
	93Ø	12	16		7Ø		1644						
	930	12 17	21	15 17	71 76		1532						м
	93Ø 93Ø	17	21	17	78		1644						
			44	10	74		1588						
											210		
•	1 8/8/1	44	1.1	13	81					120	170	407	п
							Ø Ø		Ø Ø				
							κ,	(2)		174	219.	マムフ	
		k	EV-O	F 904	AK CON	וזדזמו	3NS						
					Tmp						Star	tina	
					Air								
		70			71								
2		72			72						1		
3		76			76						- 1		
4	108	78	111		78	159	115	780			1		
5	157	75	1Ø1	109	78 77	160	115	760	SN		4		
6			103	114	81	165		810			2		
								Ø	•		_		
			EY-OF	F S04	AK ACC	ELER	POLITA	3					
Run#	15-	-50	15-	-6Ø	15-	70	Surg	RVP	T2Ø	T2ØA			
	Time	%Inc	Time	%Inc	Time	%Inc							
	142	13	275	26	472 411 51Ø	29		1669	1Ø11	1008			
2	131	4	241	1 2	411	12		1585	1Ø42	1028			
3	130	3	244	12	510	39	Т	1711	997.	955.			
4	159	26	258	18	465	27	H	1653	1017	961.			
5					555								
6	171	36	267	22	439	2Ø	Н	1609	1033	956.			
		Ø		Ø1		Ø			Ø	Ø			
					CONDIT								
					Tmp								
					Air						sec	RSt#	
					71		127						
					73				SN				
ত 4		76 79		118 120		149		765	SN				
# 5		79 78	1Ø5 1Ø1		79 79		151 157		SN SN				
5		81	105		81		160						
3	170	0.1	1%0	124	O.7	13/	1 0%,	916	214				
			IDLE	SOAK 4	ACCELE	RATIO	1NS						
					15-					T26A			
					Time								
	142	13	233		430				1013	1006			
2	158	25	240	1.0	461	26		1566	1049	1028			
3	206	63	300	37	485	32	Н	1679	1Ø11	965.			
4		50	260	19	461 485 415	13	Н	1609	1033	970.			
5	262	1Ø8	370	69	551	5Ø	н	1659	1Ø15	955.			
6		198		51	476		Н						
		Ø		وَا		Ø			Ø				
NOTES:													
					リ/L &		Air Te	emp ar	e ded	; Fx19	ð;		
6	accel (⊋ratio	on ti	nes ar	re sec	:.::1Ø							

1982 CRC Alternate Vapor Lock, Hot

Car#:			Temp (=.7ØF	-/1.Ø	=		Commer			
Run#	Date	Drvr	Obsr	F 21	AirT	Wind	RVP	T2Ø	T2ØA	Acce	lerat:	ions~	Surg
	1015	1			92					76			T
2	1015	1	11 11	8	94					84			т
3	1015	1	11	4	91					79	157	224	
							Ø Ø	Ø Ø					
							Ø	_					
							ø	ø					
							Ø	-					
							•	•	_	79.7	158.	225	
~~~~~			KEY-OF	FF SO	ak con	VDITIC	JNS			~~~~			
			a Sta										,
			TCA	TcB		TcA	TcB						
	388	92			93			925			5	2	
2	387	94			94			940			2		
3	389	91			90				SC		2		
								Ø					
								Ø					
								Ø					
			KEY-OF	:= 90/	אי ארנ	'EI ED/	ארז דנ	ø 3					
Run#	0-	-30	Ø-	-50	0	-60	Sura	RUP	T20	T20A	•		
	Time	%Inc	Time	%Inc	Time	%Inc							
			212								•		
2			212										
3	77	-3	175	11	237	5	H.	975	1346	1377			
		Ø		Ø		Ø			Ø				
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø	_			
		Ø		g Soor	30ND 73	Ø			Ø				
			IDLE S									ting	
			TcA									RSt#	
1	391	95	, 57	, w. a.'	95			950				1	•
2	378	93			93			930	SC		_	•	
3		91			91			910			2	1	
								Ø					
			•					Ø					
								Ø					
								Ø					
~~~~			IDLE										
			Ø-					RVP	T2Ø	T2ØA			
	71		Time 169	71nc	235			1.670	1707	17/17			
1 2	92 82	-11 3	255		325			1Ø39 1177					
3	76	-5	151	~5	221			974					
.	, 0	Ø		Ø		Ø	•	,,,	Ø	13/3 Ø			
		ø		ø		ø			ø	Ø			
		ø		ø		ø			ø	ø			
		ø		Ø		ø			ø	ø			
NOTES	- Runs	inc:	luded	in be	se ac	celer	ation	n time	aver	agesi	A11		
F	RVP I	s pai	100;	T92Ø	//L &	Avg A	ir Te	emp ar	e dec	Fx18	7;		

1982 CRC Alternate Vapor Lock, Hot

Car#:	14	•							ata (Commer	nts: N	10	
		•	Temp (Adjust	tment	=.7ØF	-/1.ØF	=					
Run#	Date	Drvr	Obsr	Fuel	AirT	Wind	RVP	T2Ø	T2ØA	Acce:	 lerati 0-50	ons-	Surg
1					91			1226					
2	1016	11	7	11	9ø						124	164	
											114		
4	1016	11	7	15	93		1532	1062	1076	54	124	162	
ŕ			-				Ø						
							Ø	ø	Ø				
					-		Ø	Ø	Ø				
							Ø	Ø					
									Avg:	55	120.	161.	
			KEY-OI	FF SO	ak col	NDITION	פֿענ						
	Smp#	-Tmp	a_St	art	Tmp	o ao Ei	19	Avg	Sky	Wind	Star	ting	
		Air	TCA	TCB	Air	TCA	ICB	AIT			sec	バンて #	
	376			119	91		154	919 9 9 5	SN		4 2		
2	368	9Ø 92			91 92			92Ø			3		
<u>ح</u>	228	92 93			72			925			3		
4	547	93			92				214		J		
				-				Ø Ø					
								Ø					
			VEV_0	EE GO	AK AC	TEI ER	TIONS						
Run#					Ø-						•		
					Time						•		
1	57				204								
2													
3	55	Øī	115	-4	16Ø 184	14	Н	1429	1106	1127			
4	60	9	122	2	218	36	н	1500	1075	1093			
		Ø		Ø		Ø			Ø	Ø			
		Ø		Ø		Ø			Ø				
		Ø		Ø		Ø				Ø			
	Smp#	-Tmp	a st	art	Imb	o 9 Eu	1d	Avg	Sky	Wind	Star		
_					Air	TCA	TCB	AIT			sec	RSt#	
1	383	9Ø	133	110	90		144		SN				
2		91 93			91 93			91Ø 93Ø	SN				
ى 4	_				73 92			73ø 92ø	SN				
7	J-7/	72			72			9	J. 1				
								ø					
								ø					
			IDLE S	SOAK (ACCEL	ERATIO)NS						
Run#	Ø	-3ø	Ø	-5ø	Ø-	-6Ø	Surg	RVP	T2Ø	T2ØA			
					Time								
1	56	2		-1	163	1			1218				
2	50	9		2	172	7		1270					
3	59				239		Н						
.1	62	13	130		368		Н	1415			,		
		Ø		Ø		Ø			Ø	Ø			
		Ø Ø		Ø		Ø			Ø	Ø			
NOTES	, P	_		ø,		_		, +1	-	_	. Δ11		
					//L&.								
			on ti								- •		

Acceleration times are sec.x10

1982 CRC HOT DRIVEABILITY SUMMARY (Cooperative Laboratory Data)

	# Day							
Car#	Ø1, Drvr# 1Ø	Driving Demerits	TWD	Fuel	RVP	AirT	T2Ø	%158
		Hes Stmb Surg Bkfr Stll		#	Ava	Ava	Ava	Avg
	24 8	252 702 460	775	2Ø	_	_	_	44.1
		78 174 4	232					28.2
	12							27.9
	1			1				20.2
•	-							
Car#	Ø2, Drvr# Ø4							
Run#	Idle Demerits-	Driving Demerits	TWD	Fuel				
	Ruff Stll ReSt	Hes Stmb Surg Bkfr Stll		#				Avg
1	39	_						44.9
2	114	12	126	17	1633	876	1Ø24	34.2
	03, Drvr# 10		T 1.15		O. 10	A · .=	TO 6	***
Run#	Idle Demerits-	Driving Demerits	IWD	Frei	RVP	AIFI	129	%12B
		Hes Stmb Surg Bkfr Stll		# 26				
	74	48 42	164					37.2
2	74	12 6	86	1,	1142	1042	1221	27.1
C	44 Day	•						
Car#	Ø4, Drvr# 17	Driving Demerits	THE	Fuel		Ai-T	TOO	7150
	Ruff Stll ReSt			#		Avg	AV0	êvg :
	39	822 828 324	891				1177	43.2
2								28.1
	36 36	6		1				23.7
	72 8		942					28.9
	· - -							
Car#	Ø5, Dr∨r# Ø4							
Run#	Idle Demerits-	Driving Demerits	TWD	Fuel	RVP	AirT	T2Ø	%158
		Hes Stmb Surg Bkfr Stll		#	Avg	Avg	Avg	Avg -
	66	732 330 32	85Ø					43.9
2	68	54 1Ø8	23Ø	5	1007	904	1326	24.0
Car#	Ø6, Dr∨r# Ø4							
		Driving Demerits						
		Hes Stmb Surg Bkfr Stll		#				Avg
	3	6						42.7
	2Ø 18	90						28.9 27.8
•	• •	66						22.5
4	21	84	INJ	•	717	1100	1002	22.0
Cart	Ø7, Drvr# 1Ø							
		Driving Demerits	TWD	Fuel	RVP	AirT	T2Ø	%158 -
	Ruff Stll ReSt			#	Ava	Ava	Ava	Ava
1		6.	22	2Ø	1282	1054	1174	40.1
2		6	4Ø	17	1319	1066	1157	29.2
3				14	1336	930	1149	29.5
_	_				-			`. •
Car#	Ø8, Drvr# 1Ø							r.
Run#	Idle Demerits-	Driving Demerits	TWD	Fuel	RVP	AirT	T2Ø	%158 :
	Ruff Stll ReSt	Hes Stmb Surg Bkfr Stll	~	#	DVA	AVG	AVG	AVG
1			Ø	20	1282	982	1174	40.1
2	1		1	17	1341	96Ø	1146	29.6
			-2261			_		-

NOTE: RVP is psi x 100; Avg air temperature & T920V/L are deg F x 10

1982 CRC HOT DRIVEABILITY SUMMARY (Cooperative Laboratory Data)

Car#	Ø9, Drvr# Ø4				
Run#	Idle Demerits-	Driving Demerits	TWD F	uel RVP	AirT T20 %158
		Hes Stmb Surg Bkfr S		# Avg	
1	56 16 2		96 376	2Ø 1259	982 1187 39.2
2	64	54 186 4	254	13 1302	926 1165 28.9
3	61	48 204 4	269	9 1209	930 1212 27.4
4	52	132	184	9 1225	906 1204 27.7
5	72	174	246	1 792	82Ø 1465 2Ø.3
Car#	09, Drvr# 10	_			
6	81		81	2Ø 1435	772 1096 46.2
_		•			
Ear#	10, Drvr# 10				
Run#	Idle Demerits-	Driving Demerits	TWD F	Tuel RVP	AirT T20 %158
		Hes Stmb Surg Ekfr 9		# Avg	
	58			20 1357	912 1135 43.1
2		666		9 1200	900 1217 27.3
	34	6 72 4	116	1 768	810 1482 19.9
4		666 6 72 4 96 7Ø8 4	766		824 1103 45.6
•	10, Drvr# 04		,		
	77	84Ø 816 248	917	20 1426	860 1100 45.8
	10, Dr∨r# 17	0-12 010 1-0	, . ,		
		24 492 72	530	201 1399	858 1114 44.7
O	20	27 7/2 /2	009	22 10//	000 1114 44.7
Car#	11, Drvr# Ø4				
		Driving Demerits	TWD F	Tuel RVP	AirT T20 %158
		Hes Stmb Surg Bkfr S			Avg Avg Avg
	36	24			902 1086 47.0
	48	4 7			936 1343 23.6
	70		70	J 762	/00 1040 2010
Ear#	12, Drvr# 1Ø				
		Driving Demerits	TWD F	TUEL RVP	AirT T20 %158
		Hes Stmb Surg Bkfr S			Avg Avg Avg
	31	714 7Ø2 332	793	20 1148	
2		54Ø 396 B	55Ø	5 952	1032 1360 23.1
3		138 18 6			
4		492 186 12 =	578	9 1:176	924 1230 26.9
	77	42 684 28 6			858 1126 43.8
	12, Drvr# Ø4	72 667 26 6	701	22, 10,0	000 1120 40.0
	104	756 594 268	884	201 1 1 1 1 5	830 1091 46.5
		/36 374 200	007	22/ 1440	50% 1971 46.5
	12, Drvr# 17	770 400 004	0.0	20 1400	804 1117 44 8
/	52	732 498 296	812	ZW 1488	884 1113 44.8
Car#	13. Drvr# Ø4				
		Driving Demerits	TWN =	cuel eus	Airt T20 9150
		Hes Stmb Surg Bkfr S			Avg Avg Avg
	unit acit wear	hes simb surg bktr s	L	7 PYG	932 1231 24.8
- 1 2		24	24		984 1258 34.3
		47	47	EW 1104	707 1200 04.0

NOTE: Avg RVP is psi x 100; Avg air temperature & T020V/L are deg F x 10

1982 CRC HOT DRIVEABILITY SUMMARY (Cooperative Laboratory Data)

Car#	14, Drvr# Ø4		•.
		Driving Demerits	TWD Fuel RVP AirT T20 %158
	Ruff Stll ReSt		# Avg Avg Avg Avg
		582 744 276	804 10 1108 1026 1267 25.7
Z	36 36	240 294 92	360 6 976 1062 1345 23.5
	30 30		112 9 1216 902 1209 27.5
3	<u> </u>	=	
4			48 1 779 812 1474 20.1
	39	3Ø6 282 84	393 20 1444 804 1091 46.5
6	5 7	384 390 64	567 20 1394 888 1116 44.5
Cart	15, Drvr# <i>0</i> 4		
		Driving Domorite	TWD Fuel RVP AirT T20 %158
		Hes Stmb Surg Bkfr Stll	
		24 36 44 64	214 20 1310 912 1159 41.2
2	37 24 4	6 6 200 32	101 17 1299 900 1166 28.9
Car#	16, Drvr# 17		
		Driving Demerits	TWD Fuel RVP AirT T20 %158
		Hes Stmb Surg Bkfr Stll	
	49	204 342 228	445 20 1430 920 1098 46.0
	34	6 4	44 5 996 918 1333 23.8
- 4	34	6 7	, , , , , , , , , , , , , , , , , , , ,
	17, Drvr# 1Ø		•
Run#	Idle Demerits-	Driving Demerits	TWD Fuel RVP AirT T20 %158
	Ruff Stll ReSt	Hes Stmb Surg Bkfr Stll	# Avg Avg Avg Avg
	94	3Ø	124 20 1367 928 1130 43.5
2	144 24 27		179 17 1579 878 1044 33.4
Car#	17, Drvr# 17		• • • • • • • • • • • • • • • • • • • •
	91	48 54	151 20 1401 936 1113-44.8
	18, Drvr# Ø4-		
Run#	Idle Demerits-	Driving Demerits	TWD Fuel RVP AirT T20 %158
	Ruff Stll ReSt	Hes Stmb Surg Bkfr Stll	# Avg Avg Avg Avg i
	51	6 4	61 20 1281 842 1175 40.1
	37	6	43 17 1573 864 1046 33.3
-	37	3	2
Car#	19, Drvr# 17.	-	· ·
			TWD Fuel RVP AirT T20 %158
		Hes Stmb Surg Bkfr Stll	
	36	3Ø 8	70 20 1409 898 1109 45.1
_	36 36	18 8	62 5 1941 926 1306 24.6
	⇔ 0	10	

NOTE: Avg RVP is psi x 100; Avg air temperature & T020V/L are deg F x 10

1982 CRC (1975) HOT START & DRIVEAWAY SUMMARY (Cooperative Laboratory Data)

Run#	Ø1, Drvr: 10 Idle Demerits- StTm Ruff Stll 23	Hes Stmb		#	Avg Avg	T20 %158 Avg Avg 1468 20.3
Run# 1	Ø2, Drvr: Ø4 Idle Demerits- StTm Ruff Stll 82 86		Surg Bkfr Stll	# 130 20	Avg Avg 14Ø7 888	T20 %158 Avg Avg 1110 38.7 1070 32.4
Run# 1	03, Drvr: 10 Idle Demerits- StTm Ruff Stll 21 49	Hes Stmb	Surg Bkfr Stll 8	# 47 2Ø	Avg Avg 1359 930	
Run# 	05, Drvr: 04 Idle Demerits- StTm Ruff Stll 2 86 80	Hes Stmb 12 132	Surg Bkfr Stll 60 98	# 324 20	Avg Avg 1426 923	T2Ø %158 Avg Avg 11ØØ 39.3 1348 23.4
Run# 1 2	Ø7. Drvr: 1Ø Idle Demerits- StTm Ruff Stll 33 33		Surg Ekfr Stll 28 64	#	Ava Ava	Ava Ava
	97, Drvr: 94 46	6 12	20 64	136 1	874 938	1410 21.8
Run# 1 2	1 76	Hes Stmb	ng Demerits Surg Bkfr Stll 16 224 8 160	# 326 2Ø	Avg Avg 1394 900	
Run#	10, Drvr: 10 Idle Demerits- StTm Ruff Stll -23		Surg Bkfr Stll	#	Avg Avg	T2Ø %158 AVg AVg 1Ø75 39.7
Run# 1 2		Hes Stmb 96 150 18 36	Surg Bkfr Stll 36 64 8	# 259 20 115 5	Avg Avg 1461 870 1036 880	Avg Avg 1083 40.5 1309 24.5
7 THE 7 THE B	9 13 931	n american many		a w ruany.	- are ued	, ,; 1 X*

1982 CRC (1975) HQT START & DRIVEAWAY SUMMARY (Cooperative Laboratory Data)

Run#	14, Drvr: @4 Idle Demerits- StTm Ruff Stll 7 56 31	Driving Demerits Hes Stmb Surg Bkfr Stll 108 84 32 192 24	 374	# 2Ø	Avg 1376	Avg 933	Avg 1125	%158 Avg 37.6 25.1
Car#	16, Drvr: 17							
	Idle Demerits-	Driving Demerits	TWD	Fuel	RVP	AirT	T2Ø	7158
	StTm Ruff Stll	Hes Stmb Surg Bkfr Stll		#			Avg	
1	2 4Ø	96 72 48					1095	
Car#	18, Drvr: Ø7					•		
Run#	Idle Demerits-	Driving Demerits	TWD	Fuel	RVP	AirT	T20	%158 i
	StTm Ruff Stll	Hes Stmb Surg Bkfr Stll		.#				Avg
1	9 17 16	•	33		_			34.6
Car#	18, Drvr: 17						/	O-7.0
	5 15 16	6 6 4 64	107	17	1519	925	1Ø68	32.4
NOTE:	Avg RVP is psi	x 100; Avg air temperatur	e % T	[32 Ø∀/	'L are	e deg	F × 1	g .

END

FILMED

7-85

DTIC